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THE COMET HALLEY HANDBOOK

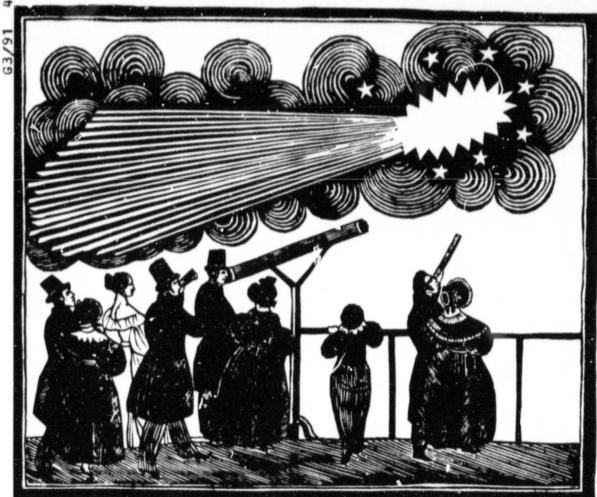
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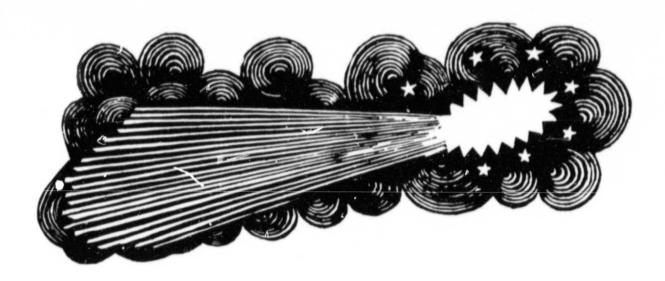


AN OBSERVER'S GUIDE



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THE COMET HALLEY HANDBOOK



AN OBSERVER'S GUIDE

CREATED FOR THE INTERNATIONAL HALLEY WATCH
BY
DONALD K. YEOMANS

JANUARY 15, 1981

Foreword

The continuing search for Comet Halley began in November 1977, when observers at two of the United States' largest telescopes unsuccessfully attempted to recover the comet more than eight years refore it is due to pass perihelion. At that time, the estimated magnitude of the comet was fainter than 26. While observations of Comet Halley at great heliocentric distances are very important for characterizing its size and physical behavior, perhaps some of the incentive for these early recovery attempts was due to the historical importance of this most famous of all comets.

Comet Halley's fame is not due to its superior brightness alone: its periodic returns every 76 years act like a clock counting time in units of human lifetimes. Thus the ever-returning comet marks transitions from one era to the next. Our parents and grand-parents have told us about the great comet's visit in 1910, and we will tell our children and grandchildren about its return in 1986. Once every 76 years, nearly everyone in recorded history has had the opportunity to view the comet.

Because of the unfavorable positions of the comet with respect to the earth and the sun, the coming apparition of Comet Halley will disappoint much of the waiting public. Comet Halley will not be an obvious naked-eye object. In fact, it will probably be invisible to the naked eye if the observer is located in a populous area with significant artificial lighting. Successful observers will have to equip themselves with binoculars, know where and when to observe, and seek an observing location free from aerial pollutants and artificial lighting.

Many will not make the effort. However, the curious will gladly go out of their way to pursue this once-in-a-lifetime experience. It is for these curious few, as well as for the small army of serious amateur and professional astronomers, that this Handbook is intended.

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The Comet Halley Handbook: An Observer's Guide

I. The Orbit of Comet Halley

Considerable portions of information in this handbook are based upon a previous work on Comet Halley's orbit, (1) The orbit determination technique used in that publication was a least-squares adjustment of the comet's motion to observational data. The observational data on Comet Halley began with a rather crude naked-eye observation by Johannes Kepler on September 28, 1607, continued through the 1607, 1682, 1759, 1835–36, and 1909–11 apparitions, and ended with a precise telescopic observation on May 24, 1911. A total of 885 observations were used in the orbit determination process. The required numerical integrations were run over various observational data arcs, with perturbations or accelerations from all nine planets taken into account at each half-day time step.

Forces other than gravity acting on a cometary nucleus often introduce an additional acceleration in its orbital motion. These so-called nongravitational accelerations are believed due to the outgassing rocket effect of the comet's ich nucleus. (2) These effects have been successfully modeled by Marsden, Sekanina, and Yeomans. (3) Yeomans included them in his computations for Comet Halley. (1)

To provide a prediction for Comet Halley's motion in 1985-86, an orbit determined from the 1759, 1835-36, and 1909-11 observations was integrated forward in time. The complete set of osculating orbit elements for 1986 is given as follows:

Epoch	1986 Feb. 19.0 (E.T.)
T	1986 Feb. 9.6613 (E.T.)
q	0.587096 (AU)
e	0.967267
ω	111.8534
Ω	58.1531
<i>t</i>	162.2378

These orbital elements are strictly correct only for a given instant of time (Epoch). However, for many low-precision computations, they can be used for several months on either side of perihelion passage T. The epoch and perihelion passage time are given in ephemeris time (E.T.). The perihelion distance and eccentricity are denoted q and e respectively. The three angular elements are the longitude of the ascending node Ω , the argument of perihelion ω , and the orbital inclination i; they are referred to the mean ecliptic and equinox of 1950.0 and are illustrated in Figure 1.

Figure 2 illustrates an ecliptic plane projection of Comet Halley's orbit within the solar system. Figure 3 illustrates the relative positions of the comet and earth in the 1985-86 time period. The pre- and post-perihelion close approaches of the comet and earth occur on November 27, 1985 and April 11, 1986 at minimum distances of 0.62 and 0.42 AU respectively. The position of the vernal equinox on Figures 1, 2, and 3 is

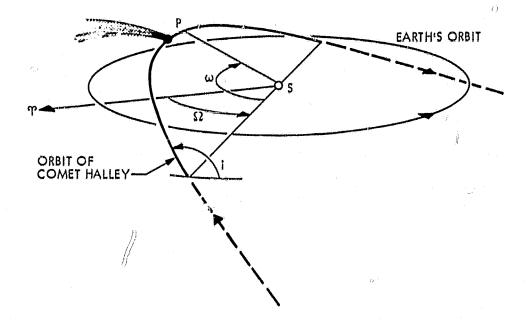


Fig. 1. Angular Elements of the Orbit of Comet Halley. For Comet Halley, the Orbital Inclination I is 162°, the Longitude of the Ascending Node Ω is 58°, and the Argument of Perihelion ω is 112°.

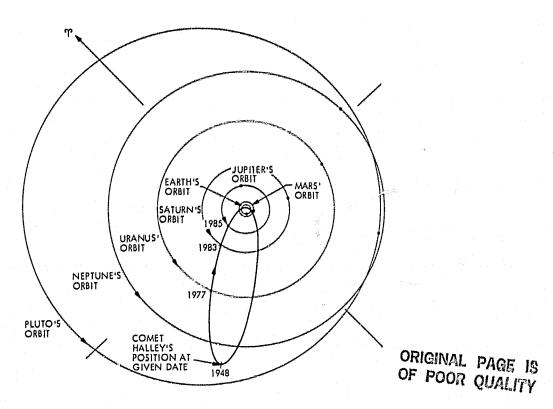
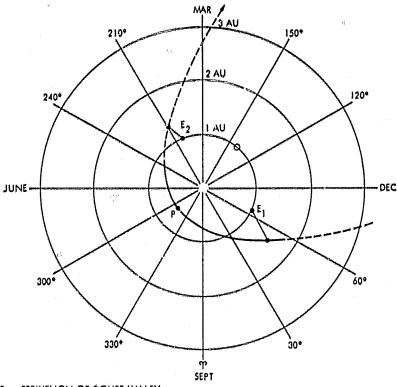


Fig. 2. Ecliptic Plane Projection of Comet Halley's Orbit (1910—1986) Within the Solar System.

The planetary positions are indicated for the time of the comet's perihelion passage.



P = PERIHELION OF COMET HALLEY

E, = POSITION OF EARTH AT PRE-PERIHELION CLOSE APPROACH OF COMET (NOV. 27, 1985)

E POSITION OF EARTH AT POST-PERIHELION CLOSE APPROACH OF COMET (APR. 11, 1986)

O = POSITION OF EARTH AT PERIHELION OF COMET HALLEY (FEB. 9, 1986)

Fig. 3. Relative Positions of Comet Halley and Earth, 1985-1986.

denoted by the symbol T. Figure 4 shows the comet's path through the constellations for the period November 1985 through May 1986.

II. The Expected Physical Behavior of Comet Halley in 1985–1986

Like other active comets, Comet Hailey's physical behavior is likely to change markedly from day to day. Anyone who attempts to predict the physical behavior of an active comet is almost certain to be incorrect. Nevertheless, an analysis of Comet Halley's physical behavior during the past few apparitions has been included in the hope that this information will serve as a rough guide to the comet's behavior in 1985-86. In an effort to predict the comet's apparent brightness, tail lengths, and coma diameters in 1985-86, an analysis of existing data is presented in the following subsections.

A. Brightness Estimates

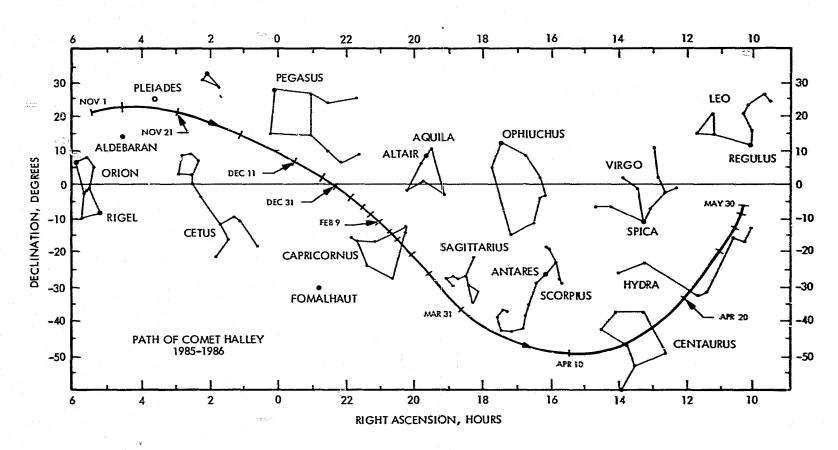
Visual magnitude estimates of a comet depend upon the subjective judgment of the observer, the brightness of the

night sky, and the aperture size of the telescope employed. For the present analysis, no observer-dependent corrections or night-sky corrections could be made with the existing data. Using an empirical correction of 0.055 magnitudes per cm for refracting telescopes, the magnitude estimates made with the naked eye and telescopic apertures <33 cm were normalized to a standard aperture of 6.78 cm. (4) Since only magnitude data from refracting telescopes were used, a separate normalization law for reflecting telescopes was not required. Where magnitude data were taken with telescopic apertures greater than 33 cm, no normalization was attempted. The value 0.055 magnitudes per cm completely breaks down for large-aperture telescopes, and insufficient data were available for establishing a normalization of Comet Halley magnitude data made with large-aperture telescopes.

Traditionally, the total apparent magnitude M_1 of a comet is expressed as

$$M_1 = M_0 + 5 \log \Delta + n \log r \tag{1}$$

where Δ and r are respectively the geocentric and heliocentric



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Fig. 4. Path of Comet Halley on the Celestial Sphere During November 1985—May 1986.

distance of the comet in AU, and M_0 is the total absolute magnitude of the comet ($M_1 = M_0$ when $\Delta = r = 1$). Figure 5 illustrates 1909-1910 visual apparent magnitudes plotted in a form $M_1 = 5 \log \Delta$ vs. $\log r$. For 1910, the intrinsic brightness of Comet Halley as a function of heliocentric distance was not symmetrical with respect to perihelion. Pre-perihelion, the total magnitude can be represented by the following formula of standard form:

$$M_1 = 5.0 + 5 \log \Delta + 13.1 \log r$$
 (2)

Post-perihelion, the total magnitude is first fainter and then substantially brighter than corresponding pre-perihelion magnitudes at the same heliocentric distance. While Comet Halley's post-perihelion brightening is well established, the 1910 post-perihelion brightness dip between 0.6 and 1 AU may have been due in part to the comet's relatively low clongation angles (i.e., the M_1 estimates were not made in a completely dark sky). Data gaps, due to small solar elongation angles, are present for -0.23 < log r <0.02 (pre-perihelion) and for 0.33 < log r <0.51 (post-perihelion). The pre- and post-perihelion brightness curves in Figure 5 should be useful for predicting observed total magnitudes in the coming apparition of Comet Halley. The apparent total magnitude estimates predicted in Appendix B were computed by evaluating curve fits of the data in Figure 5.

A separate analysis was conducted using brightness estimates that were described in the literature as nuclear magnitudes. Nuclear magnitude estimates M_2 made in large telescopes at great heliocentric distances were analyzed. The data used was photographic and could be fit with the following formula:

$$M_2 = 7.5 + 5 \log \Delta + 10 \log r$$
 (3)

However, the earliest pre-perihelion observation of Comet Halley was made at r = 3.6 AU on August 25, 1909 and the latest post-perihelion observation was made at r = 5.4 AU on June 16, 1911; outside this range in heliocentric distance, the M_2 values presented in Appendix B are only extrapolated estimates. True nucleus brightness, as opposed to the apparent or photometric nucleus, must follow a 5 log r behavior, of course.

B. Tail Lengths

To obtain some idea of Comet Halley's tail evolution with heliocentric distance r, we collected apparent tail-length data for the last three apparitions. Only naked-eye, angular, tail-length estimates were used in our analysis, and the assumption was made that the tail was always directly anti-solar. This latter assumption is somewhat in error for dust tails, but the

subjective nature of the tail-length estimates did not seem to warrant a more comprehensive analysis. Using the comet's solar-elongation angle β and the geocentric distance of the comet Δ , the actual, linear tail length s may be computed from the apparent (foreshortened) angular tail length t by

$$s = \frac{\Delta \sin t}{\sin (\beta - t)} \tag{4}$$

The linear tail lengths s, plotted as a function of heliocentric distance, are presented in Figure 6. While the actual tail lengths observed will depend upon the observing conditions and the optical instrument used, the shape of the curve in Figure 6 is suggestive. Comparing the 1759, 1835, and 1910 data, the comet's visual tail length appears to be longest after perihelion.

C. Coma Diameters

Figure 7 presents the linear coma diameters determined from visual observations made in 1909-11. The observed angular coma diameters, in each case, were multiplied by the geocentric distance of the comet at the time of observation to obtain the linear coma diameters. Note that the coma diameter reached a maximum value of approximately 200,000 km just after perihelion. Because the actual coma diameters will depend on the optical instrument used to observe the comet, the data given in Figure 7 are crude. Nevertheless, the curve does indicate the general evolution of the coma diameter with heliocentric distance.

III. Observing Conditions for Comet Halley in 1985–1986

As is evident from Figures 3 and 4, the changing positions of the comet and earth in 1985-86 will cause different observing conditions for the comet before and after perihelion. In general, the pre-perihelion positions of Comet Halley will allow better observing conditions for northern hemisphere observers, while southern hemisphere observations will be preferred post-perihelion.

For a given day, the comet's observability will depend upon the observer's latitude. We have assumed that the comet will be visible to an observer if the comet is above, and the sun is simultaneously more than 18° below the local horizon. This condition assures that evening astronomical twilight has ended and morning astronomical twilight has not yet begun (i.e., the comet is seen in a dark sky). The time interval for which this condition holds is referred to as the number of available dark hours. Figure 8 plots the available dark hours vs. calendar date for an observer at 35° N and 35° S latitude. Also plotted in Figure 8 is the total apparent magnitude M_1 vs. calendar date. Table 1 lists the dark hours vs. calendar date for observers

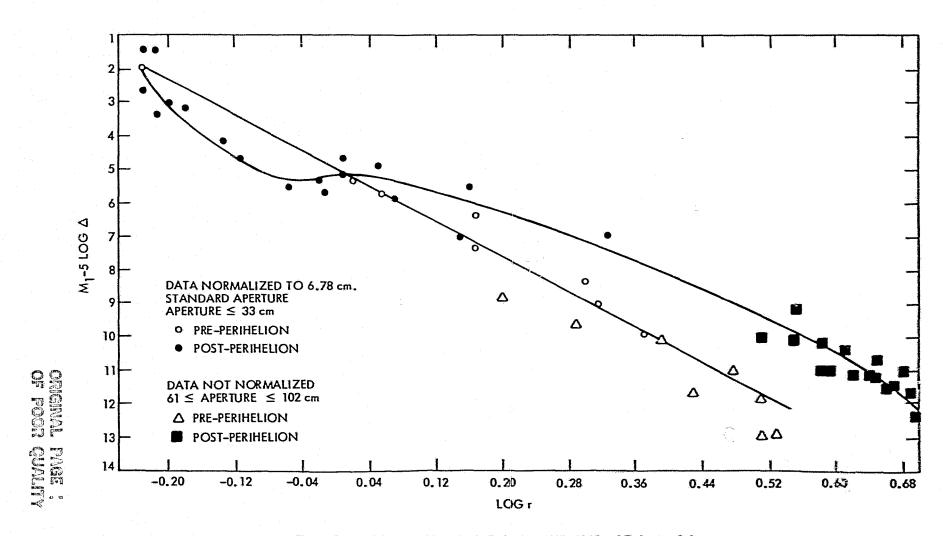


Fig. 5. Comet Halley Total Magnitude Estimates, 1909-10 Visual Estimates Only

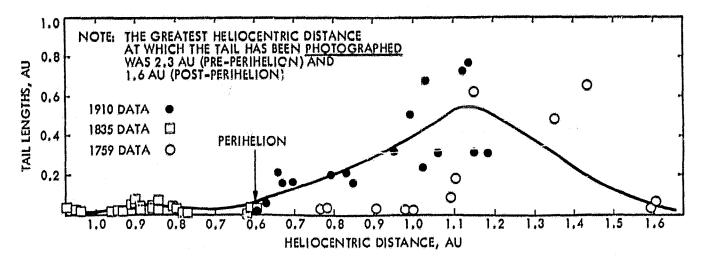


Fig. 6. Comet Halley Lines: Vall Lengths Computed from Naked-Eye Estimates.

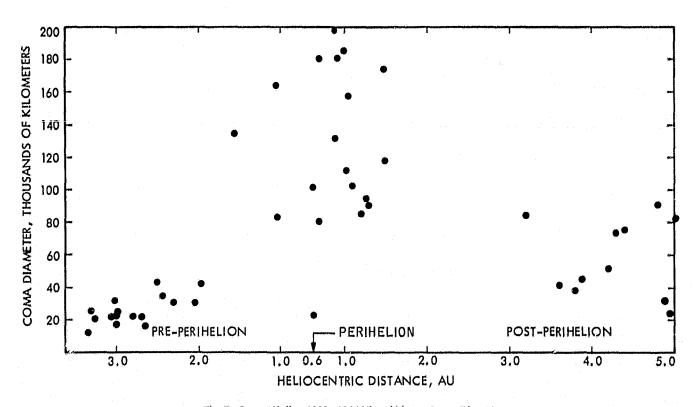


Fig. 7. Comet Halley 1909-1911 Visual Linear Coma Diameters.

located at 45°N, 30°N, 30°S, and 45°S. Table 1 also gives the predicted apparent total M_1 and nuclear M_2 magnitudes of the comet as a function of calendar date.

Figures 9.13 are schematic representations as to how Comet Halley may appear on various dates for observers located at latitudes of 40°N, 30°N, 20°N, 20°S, and 30°S.

The comet's elevation above the local horizon and its azimuth (degrees east of north) are given for various dates. For each date, the comet's position is given for the end of astronomical twilight if the comet is in the evening sky, or the beginning of astronomical twilight if the comet is in the morning sky. These positions correspond to times approximately 70-90 minutes after sunset or 70-90 minutes before sunrise. Very

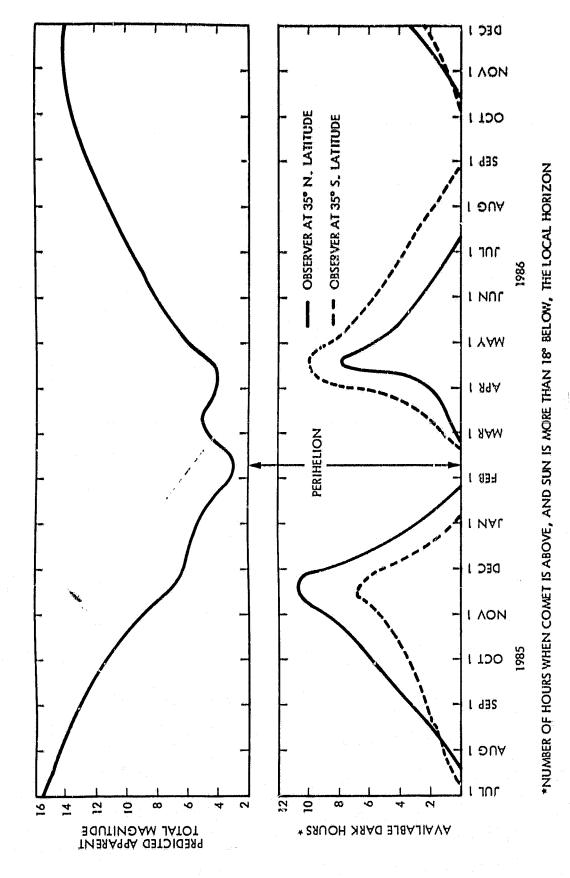


Fig. 8. Comet Halley 1985 → 1506 Ground-Based Observing Conditions.

Table 1. Ground-Based Observing Data, Comet Halley 1985-1986.

Dark Hours					rent			****	llours	*******	Apparent Magnitudes		
Date (198)	North	Lat.	South	Lot.		tudes	Date (1986)	North	Lat.	South	Lat.		
Duca (130)	45°	30*	30°	45*	Ml	M ₂	Date(1900)	45*	30°	30*	45*	M1	М2
Jan. 1	11.6	10.9	6.8	3.5		17.9	Jan. 6	2.6	2,3	0.5	0	5.1	7.7
11	10.7	10.0	6.9	3.9		17.8	16	1.3	1.1	0	0	4.4	7.2
21	9.7	9.1	7.2	4.6		17.7	26	0	0	0	0	3.6	6.7
31	8.7	8.1	5.6	5.3		17.7	Feb. 5	0	0	0	0	3.0	6.2
Feb. 10	7.7	7.2	5.0	3.7		17.6	15	0	0	0	0	3.1	6.2
20	6.8	6.4	4.4	3.3		17.6	25	0	0.3	0.7	0.5	4.3	6.4
Mar. 2	5.8	5.5	3.9	2.9		17.5	Mar. 7	0.2	0.9	2.0	2.0	5.0	6.8
12	4.9	4.7	3.4	2.5		17.5	17	0.5	1.5	3.3	3.7	4.8	7.0
22	4.0	4.0	2.9	2.1		17.4	27	0.7	2.3	5.3	6.2	4.3	6.9
Apr. 1	3.2	3.2	2.4	1.8		17.4	Apr. 6	0	3.8	9.1	9.4	4.0	6.7
11	2.3	2.5	1.9	1.4		17.3	16	6.0	8.3	10.0	9.9	4.4	7.2
21	1.4	1.7	1.5	1.0		17.2	26	6.2	8.0	9.2	10.0	5.5	8.5
May 1	0.5	1.0	1.0	0.6		17.1	May 6	5.5	5.1	7.7	8.3	6.5	9.7
11	0	0.3	0.5	0.2		17.0	16	2.7	4.3	6.7	7.3	7.3	10.7
21	Ó	0	0	0		16.8	26	1.9	3.5	გ.0	6.5	7.8	11.4
31	Ö	0	/ O	0		16.7	June 5	1.0	2.8	5.3	5.8	8.3	12.2
June 10	Õ	0 //	Ö	ő		16.5	15	0.2	2.1	4.6	5.1	8.8	12.8
20	õ	0	Õ	Õ		16.3	25	0	1.5	4.0	4.5	9.3	13.3
30	Õ	Ö	Ö	Õ		16.1	July 5	Ŏ	0.9	3.4	Š.9	9.8	13.8
July 10	ō	ō	0.3	0.1		15.9	15	Õ	0.4	2.7	3.2	10.3	14.2
20	ŏ	0.5	0.8	0.5	14.8	15.7	25	Ö	Ō	2.1	2.5	10.8	14.6
30	0.5	1.2	1.3	0.9	14.4	15.4	Aug. 4	0	Õ.	1.5	1.9	11.3	14.9
Aug. 9	1.4	1.9	1.7	1.3	14.1	15.1	14	Ö	Õ	0.9	1.2	11.8	15.2
19	2.3	2.6	2.1	1.6	13.7	14.7	24	õ	Ö	0.3	0.5	12.3	15.5
29	3.2	3.3	2.5	1.9	13.2	14.4	Sept. 3	Ö	ŏ	0	0	12.7	15.7
Sept. 8	4.1	4.0	2.9	2.2	12.7	13.9	13	Õ	ŏ	ŏ	ő	13.1	16.0
18	5.0	4.8	3.3	2.5	12.2	13.5	23	ŏ	ŏ	ŏ	ŭ.	13.4	16.2
28	5.9	5.6	3.8	2.8	11.6	12.9	Oct. 3	Ŏ.	Ö	ŏ	Õ	13.6	16.3
Oct. 8	6.9	6.4	4.3	3.1	10.9	12.3	13	Ö	0.1	0.4	ő	13.8	16.5
18	8.0	7.3	4.9	3.5	10.1	11.6	23	0.4	0.8	0.8	ŏ.4	13.9	16.6
28	9.2	8.5	5.7	4.1	9.3	10.8	Nov. 2	1.2	1.5	1.2	0.7	14.0	16.8
Nov. 7	10.7	10.0	6.8	5.0	8.3	10.0	12	2.0	2.2	1.7	1.0	14.1	16.9
17	11.1	10.6	7.3	4.9	7.2	9.0	22	2.7	2.8	2.3	1.4	14.1	16.9
27	10.6	9.8	7.0	4.2	6.4	8.4					* • •	****	.~./
Dec. 7	7.7	7.1	4.4	3.6	6.1	8.1							
17	5.5	5.1	2.8	1.0	5.9	8.1							
27	3.9	3.6	1.5	0	5.6	8.0							
21	2,9	5.0	1.00	U	٠.٠	0.0							

Note: (1) For a particular observer's latitude, the number of dark hours is defined as the time interval during which the sun is below the local horizon by at least 18 degrees and the comet is simultaneously above the local horizon.

rough indications of the comet's tail length and orientation are given for a few representative dates along with the comet's apparent total magnitude M_1 in parenthesis. The tail-length estimates presented in Figures 9 through 13 were obtained by solving for t in formula (4) and using the data in Figure 6 and

Appendix B. Only the period when the comet is brightest (January-April, 1986) is represented on Figures 9-13. Note that the comet passes near opposition in April 1986; for some latitudes, it is then observable as both an evening and morning object.

⁽²⁾ Magnitude estimates are based upon the comet's observed behavior in 1909-10. Predictions are for ideal observing conditions.

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Fig. 9. Comet Halley Observing Conditions in 1986 for Observers Located at 40° North Latitude. Comet Positions are Given for Beginning of Morning Astronomical Twilight or End of Evening Astronomical Twilight. Approximate Total Visual Magnitudes are Given in Parentheses Following Dates. Viewing with Binoculars and Ideal Observing Conditions are Assumed.

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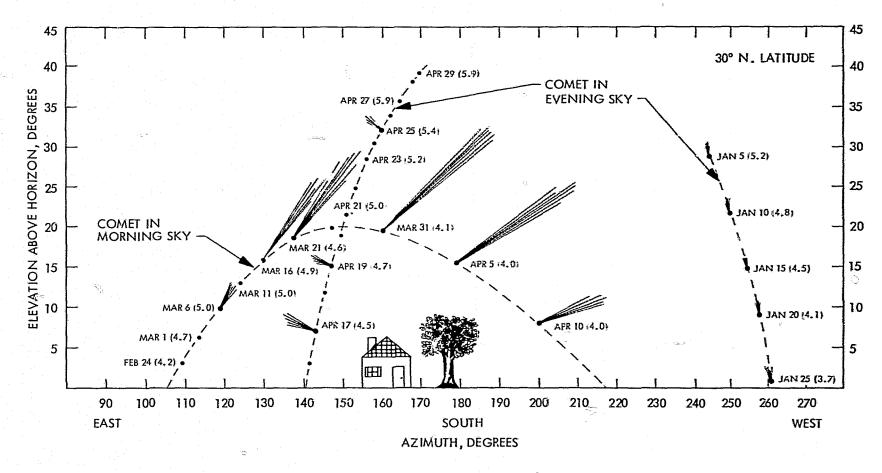


Fig. 10. Comet Halley Observing Conditions in 1986 for Observers Located at 30° North Latitude. Comet Positions are Given for Beginning of Morning Astronomical Twilight or End of Evening Astronomical Twilight. Approximate Total Visual Magnitudes are Given in Parentheses Following Dates. Viewing with Binoculars and Ideal Observing Conditions are Assumed.

Fig. 11. Comet Halley Observing Conditions in 1986 for Observers Located at 20° North Latitude. Comet Positions are Given for Beginning of Morning Astronomical Twilight or End of Evening Astronomical Twilight. Approximate Total Visual Magnitudes are Given in Parentheses Following Dates. Viewing with Binoculars and Ideal Observing Conditions are Assumed.

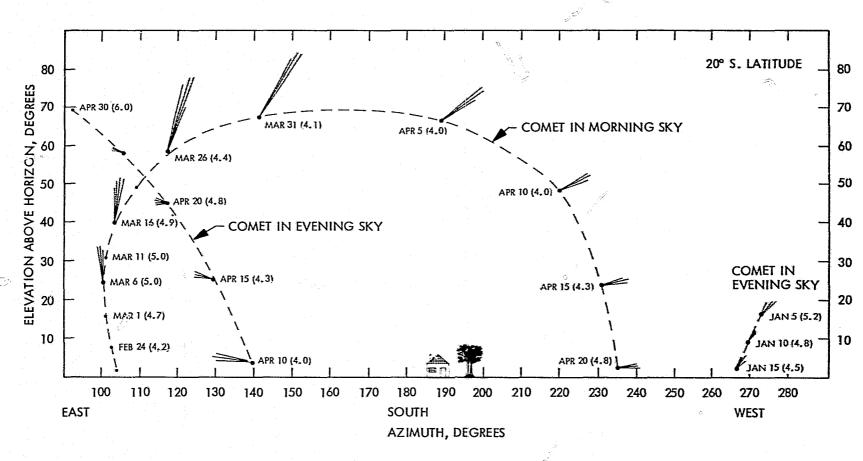


Fig. 12. Comet Halley Observing Conditions in 1986 for Observers Located at 20° South Latitude. Comet Positions are Given for Beginning of Morning Astronomical Twilight or End of Evening Astronomical Twilight. Approximate Total Visual Magnitudes are Given in Parentheses Following Dates. Viewing with Binoculars and Ideal Observing Conditions are Assumed.

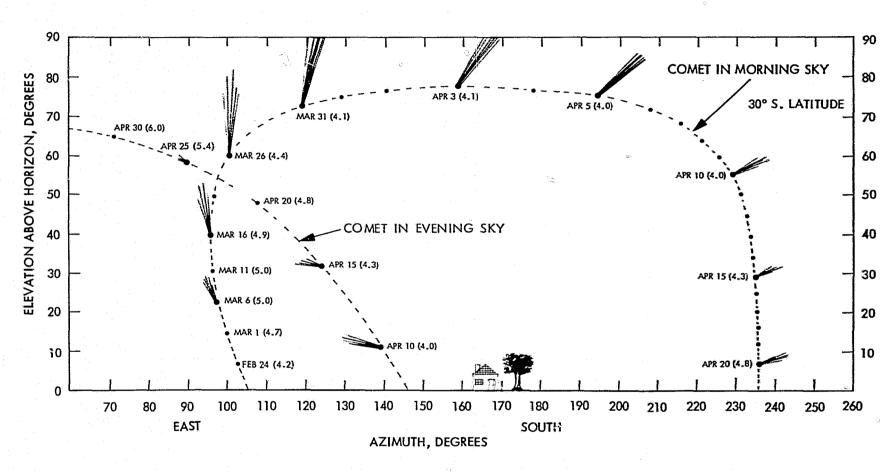


Fig. 13. Comet Halley Observing Conditions in 1986 for Observers Located at 30° South Latitude. Comet Positions are Given for Beginning of Morning Astronomical Twilight or End of Evening Astronomical Twilight. Approximate Total Visual Magnitudes are Given in Parentheses Following Dates. Viewing with Binoculars and Ideal Observing Conditions are Assumed.

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Appendix A

Historical, Physical, and Orbital Data

Historical, Physical, and Orbital Data

Historical Data

Earliest probable recorded apparition

240 B.C.

Number of recorded apparitions From 240 B.C. to 1910 A.D., only the 164 B.C. apparition was not recorded.

28

Shortest period between returns to perihelion

74.42 years (1835-1910)

Longest period between returns to perihelion

79,25 years (451-530)

Closest approach to the earth

0.04 AU (April 11, 837)

Longest angular tail length recorded

93° (mid-April 837)

Brightest apparent magnitude recorded

-3.5 (April 11, 837)

(approximate)

Physical Characteristics

Estimated diameter of nucleus

5 km

Estimated density of nucleus

1 g/cm³

Estimated rotation period^{A-1}

10.3 hours, direct

Observed spectra in 1910^{A-2}

CH, CN, C₂, C₃, Na D, CO⁺, N₂⁺

Observed tails

Type I ion and Type II dust

Associated meteor streams

η Aquarid (Early May) and Orionid

(late October)

Orbital Characteristics

Location of orbit pole

 $\lambda = \Omega - 90^{\circ} = 328.15^{\circ}$ $\beta = 90^{\circ} - i = -72.24^{\circ}$

Location of perihelion

 $\lambda = \Omega + \tan^{-1} (\tan \omega \cos i) = 305.32$ $\beta = \sin^{-1} (\sin \omega \sin i) = 16.45^{\circ}$

Heliocentric distance of orbit nodes

 $r(\Omega) = q(1+e)/(1+e\cos\omega) = 1.81 \text{ AU}$

 $r(\mho) = q(1 + e)/(1 - e \cos \omega) = 0.85 \text{ AU}$

Distance of perihelion and aphelion above or

below orbit plane (in AU)

 $Z(q) = q \sin \omega \sin i = 0.17 \text{ AU}$

 $Z(Q) = Q \sin \omega \sin i = 9.99 \text{ AU}$

Orbital velocity (in km/sec)

$$V = 29.8 \left[\frac{2}{r} - \frac{1}{a} \right]^{1/2}$$
$$= 29.8 \left[\frac{2}{r} - 0.0558 \right]^{1/2}$$

At perihellon r = q

At aphelion r=Q

V = 54.55 km/sec

V = 0.91 km/sec

Definitions

λ, β	ecliptic longitude, latitude
Ω, \mho	longitude of the ascending, descending node
ω	argument of perihelion
	inclination of orbit plane with respect to the ecliptic
q, Q	perihelion, aphelion distance in AU
e	orbital eccentricity
a	semimajor axis in AU

References

- A-1. Whipple, F. L., private communication, March 1, 1980.
- A-2. Bobrovnikoff, N. T. (1931) Publications of the Lick Observatory, v. 17, part II.

Appendix B

Ephemeris Data 1981-1987

Explanation of Symbols

J.D.

= Julian Date (Ephemeris Time)

R. A. 1950.0 DEC.

Geocentric right ascension and declination referred to the mean equator and equinox of 1950.0. Light time corrections have been applied

R. A. APPN DEC.

* Apparent geocentric right ascension and declination. Light time, annual aberration, and nutation corrections have been applied, and R. A. and Dec. have been precessed to the ephemeris date.

DELTA

Geocentric distance of comet in AU

DELDOT

■ Geocentric velocity of comet in km/sec

R

Heliocentric distance of comet in AU

RDOT

= Heliocentric velocity of comet in km/sec

 M_1

Total magnitude = 5.0 + 5.0*log (Delta) + 13.1*log (R), pre-perihelion. Post-perihelion, M₁ is determined empirically from the 1910-11 magnitude estimates (see Figure 5)

M₂

* Nuclear magnitude $= 7.5 + 5.0 \cdot \log (Delta) + 10.0 \cdot \log (R)$

NOTE:

In cases where M_1 is not computed, the corresponding column is filled with zeros (0.0).

= Sun-Earth-Comet angle in degrees

THETA BETA

= Sun-Comet-Earth angle in degrees

MOON

= Comet-Earth-Moon angle in degrees

NOTES:

1. The following osculating orbital elements are consistent with the following epitemeris:

Epoch	2446480.50000	1986	FEB.	19.00000 (E.T.)
Perihelion Passage	2446471.16128	1986	FEB.	9.66128 (E.T.)
Perihelion Distance in AU	0.5870959			
Eccentricity	0.9672671			The state of the s
Argument of Perihelion	111.85336			
Longitude of Ascending Node	58.15313			Afficiency of the second of th
Inclination	162.23779			

2. Angles are in degrees and are referred to the ecliptic and equinox of 1950.0.

OF POOR ONE

Table B-1. Ephemeris (with Perturbations) for Comet Halley at 10-Day Intervals from December 25, 1960 to June 8, 1962.

YR MN DY	HR	J.D.	R.A. 1950.0 I	Dec	2. 1	APPN	NEC.	DELTA	DELDOT	R	RDOT		THETA	BETA MOON
					R.A.							M ₁ M ₂		
1930 12 25 1931 1 4			7 15-465 + 7 5						-15.87 -19.41		-2.26 -5.28	.0 24.8 .6 24.8		1.4 29
1931 1 14				1.88 7			58.77		-4.85		-8.30	.C 24.7		1.1 75
1531 1 24				9.79 7	2.73			13.47		14.38	-8.32	·C 24.7		1.5 53
1,31 3			6 58 092 + E 1				16.47			14.33	-3.35	.C 24.7		2-1 166
1931 2 13			6 55.418 + 8 2				27.22		17.13		-8.37	.5 24.7		2.6 35
1931 2 23			6 53-102 + 8 4				38.78		13.94	14.24	-8.39	.C 24.7	128.3	3-1 96
1981 3 5		2444668.3	6 51-207 + 8 5	3.26 6	52.90	7 + 8	50.76	13.69	16.98	14.19	-8.42	-C 24-7		3.5 136
1981 3 15	•	2444678.5	6 49.782 + 9	5+25 6			2.82		19.11	14.14	-8.44	.C 22.7	108-5	3.8 13
1931 3 25			6 48.352 + 9 1				14.60		20.33		-5.46	·C 24.7	98.3	4.C 128
1931 4 4			6 48.420 + 9 2				25.79		23.67		-8.49	.0 24.7	58-6	4.1 99
1981 4 14			6 48.478 + 9 3				36.12		53.65		-8.51	.C 24.7	79-1	4.0 43
1931 4 24			6 49.001 + 9 4				45.34		18.73		-8.54	.0 24.7	69-7	3-9 150
1981 5 4 1981 5 14			6 49.952 + 9 5 6 51.289 +10				53.29 59.78		16.65		-8.56 -6.58	.C 24.7	60.5 51.4	3.6 62 3.3 75
1981 5 24		The second secon		7.26 6				14.52	19.59		-2.01	.C 24.7	42.6	2-9 161
1981 6 3			£ 54-912 +10 1		56.60			14.57		13.75	-8.63	·C 24.7	34.1	2.4 26
1931 6 13	-		6 57-087 +16 1		58.78			14-60		13.70	-3.66	.0 24.7	24.0	1.9 106
1931 6 2			6 59.424 +10 1			+10		14.61	-1.63		-8.68	.0 24.7	18.6	1.4 129
1981 7			7 1.864 -10 1		3.56			14.58	-6.16		-5.71	.0 24.7	13.4	1.0 16
1981 7 13	آ ء . کا	2444798.5	7 4.345 +10	7.74 7	6.04	2 -10	4.77	14.53	-15.74	13.55	-5-73	-0 24-6	13.0	1-0 135
1981 7 2	5 .	2444808.5		3.10 7					-15.25		3.76	-D 24-6	17-7	1.3 94
1981 5			7 9.179 + 7 5				- 191		-19.66		-6.79	.0 34.6	24.9	1.8 46
1981 8 17			7 11.466 + 9 4						-23.87		-5.81	.6 24.5	13.0	2.4 163
1981 8 2			7 13.423 + 9 4						-27.60		-5.84	-0 24-5	41.5	2-9 58
1981 9 1			7 15-169 + 9 3						-31.00		-8.86	.0 24.5	50-2	3.3 78
1981 9 11			7 16.581 • 9 2						-33.81 -36.01		-8.89 -8.92	.0 24.4	59-2	3.7 157 4.1 22
1981 9 21 1981 10			7 18-132 + 9			-	4		-37.30		-8.94	.0 24.3	77.8	4.3 109
1981 10 11	_		7 18.271 + 8 5						-38.15		-5.97	.0 24-3	87.4	4.4 125
1981 10 21			7 17.836 + & 4						-37.97		-9.60	.0 24.2	97.1	4.3 22
1981 10 31			\$ \$6.851 + 8 3						-36.87		-9.03	.C 24.1		4.2 140
1981 11 13			1 15.312 + 8 2						-34.83		-9.06	.C 24.1		3.9 E8
1981 11 2.		2444928.5	7 13.235 + 8 2	24.71 7	14.96	8 + 2	21.33	12.26	-31-93	12.88	-9.08	-C 22.C	127.2	3.5 56
1981 11 30		2444938.5	7 10-655 + 8 2	1.6E 7	12.38	7 + 5	18.40	12.08	-25.15	12.82	-9.11	.0 24.0		3.0 166
1981 12 13			7 7-638 + 8 2						-23.65		-9.14	-C 23-9		2.4 49
1781 12 23			7 4.273 + 8 2						-18-60		-9.17	-6 23-9		1.8 92
1981 12 30			7 .666 + 8 2						-13.23		-9.20	-C 33-9		1.2 144
1752 1 9	_		6 56.947 + 8 3				29.02		-7.52		-9.23	-0 53-E		1-1 15
1932 1 19			6 53-250 + 8 3				37.12		-1.97		-9-26	.C 23.8		1.6 126 2.2 108
1732 1 29			6 49.708 + E 4 6 46.444 + 5				47.02 58.38			12.51	-9.29 -9.32	.C 23.8		2.8 35
1932 2 : 1982 2 18			6 43 570 + 9 1				10.82		12.14		-9.35	.0 23.8		3.4 157
1982 2 28			6 41.170 + 9 2				23.93		15.44		-9.38	.C 23.8		4.C 69
1982 3 13			6 39-307 + 9 3				37.32		17.80		-9.41	-0 23-8		4.3 71
1932 3 20			6 38-012 + 9 5				50.59		17.28		-9.46	-C 23-8		4-6 160
1982 3 30		0 2445058-5	6 37-302 +10	5.29 6	39.06	+10	3.40	12.12	19.82	12.18	-9.47	-G 23-8	90.9	4.7 31
1782 4 9			6 37-166 +10 1			_	15.43		19.44		-9.50	.G 23.8	£1.2	4.7 105
1982 4 19	, ,,,		6 37-577 +10 2				26.39		18.27		-9.53	.0 23.8	71.8	4.5 131
1982 4 29			6 38-498 +10 3				36.07		16.30		-9.56	.0 23.8	62.5	4.3 15
1982 5			6 39-879 +1C 4				44.27		13.68		-9.60	-0 53-8	53.4	3.9 137
1982 5 1			6 41.661 +10 5				-	12.6G			-9.63	-0 23-8	42.6	3.4 98
1982 5 2			6 43.786 +10 5				55.72		,	11.85	-9.66	.0 23.7	35.9 27.7	2.9 47 2.3 164
1982 6 8	<u> </u>	0 2445128.5	6 46.186 +11	1.G4 6	~/.74	3 410	58.80	12.68	2+60	11.79	-9.69	-0 23.7	Cf + f	E+2 154

Table B-2. Ephemeris (with Perturbations) for Comet Halley at 5-Day Intervals from June 18, 1982 to September 30, 1984.

_	YR	MN DY	HR	J.D.	R.A.	1950.0	DEC.		R.A.	APPN	DEC.	DELTA	DELDOT	R	RDOT	H.	н2	THETA	BETA	3900M
1	983	6 18	•3	2445138.5	6 48.7	96 +11	2.42	5	50.55	5 +11	.07	12.69	-1.49	11.74	-9.73	-0	23.7	20.0	1.7	
1	1982	5 23	+0	2445143.5	6 50.1	59 +11	2.43	5	51.91	9 +11	-03	12.68	-3.73	11.71	-9.74		23.7	15.7	1.4	
3	1982	5 28	-0.	2445148.5	6 51.5	49 +11		5	53.31	+10	59.53	12.67			-9.76		23.7	13.9	1.5	
	982	7 3	- 0	2445153.5		55 +11					58.60				-9.78		23.7	12-2		143
	1982	7 8	• 0	2445158.5			59 ្គ្លូ១						-10-53		-9.79		23.7	11.9		156
	982	7 13	• 0	2445163.5		90 +10							-12.83		-7.81		23.6	13.2	1.1	
	982	7 18	• 8	2445168.5		00 +10		-					-15.07		-9.83		23.5	15.5	1-4	
	1982	7 23	-0	2445173.5		93 +10		7					-17.32		-9.85		23.6	13.5	1.6	
	982	7 28	0	2445178.5			50.45	7					-19.51		-9.86		23.6	22-4		111
-	1982	8 2	•0	2445183.5			47.16	7					-21.64		-9.88		23.6	25.2		165
	982	8 7	•0	2445185.5			43-52	7					-23.71		-9-90		23.5	30.2		126
	982	8 12	- 0	2445193.5		_	37.57	7					-25.71		-9-92		23.5	34-4	2.9	
	982	8 17	• 0	2445198.5			35.33	7					-27.63		-9.93		23.5	39.5		14
	1982	8 22	-0	2445233.5		93 +10		7					-29.45		-9-95		22.5	42.9	3-5	
	982	8 27	-0	2445238.5			25.05	7					-31.15		-9.97		27.4	47-3		141
	1982	9 1	• 0	2445213.5			21.13						-32.72		-9.99		23-9	51.7		154
	1982	9 6	-3	2445218+5			15.97						-34.15				23-4	55.2	34.3	
	1982	9 11	•0	2445223.5	7 9-6								-35.45				23.4	50.7	4.5	
	982	9 16	• 0	2445228.5	7 10.2								-36.59				23-3	65.3	4.7	
	1982	9 21	• 0	2445233.5			59.92						-37.55				23-3	59.9		112
	1982	9 26	-0	2445238.5			59.49						-38.32				23.3	74.6		165
	982		-0	2445243.5			49-08						-38.89				23.2	79.3		124
		10 6	• 0	2445248.5	7 11.3								-39.27				23-2	84.1	5.1	
		10 11	+0	2445253.5			39.55						-39.46				23.2	88.9	5.2	
		10 16	•0	2445258.5			33.52						-39.41				23.1	93.8	5.2	
		10 21	-0	2445263.5	7 10.6								-39.13				23.1	95.7		143
		10 26	•0	2445268.5			24.17						-38-61					103.7		1 153
	_	10 31	-0	2445273.5			19.95						-37.85					109.7	4-5	
	_	11 5	• 0	2445278.5			15-13						-36.88					113.8	4.8	
		11 10	• 0	2445283.5			12.66	7					-35.68					115.8	N-6	
		11 15	•0	2445288.5		77 + 9		7		8 + 9			-34-24					124-0		117
		11 20	• 0	2445293.5		83 + 9		7		5 + 9			-32.56					129.1		165
		11 25	• 0	2445298.5		34 + 9		7		8 + 9			-33.67					134.3		7 118
		11 30	•0	2445303.5		40 + 9		7		7 + 9	-99		-28.59					139.4	3.4	
		15 2	-0	2445308.5		12 + 9		7		2 + 3	-30		-26.33					144.5	3-1	
		12 10	0	2445313.5		53 + 9			59.55		-25		-23.91					149.5	2.7	
		12 15	• 0	2945318.5		36 + 9			57.51		.83		-21-32					154.3		150
		12 20	-0	2445323.5		59 + 9					2.08		-18.62					158.5		142
		12 25	- 0	2445328.5		41 + 9			53.15		3.98	, .=	-15.83					162.7	1.1	
_		12 30	-0	2445333.5		73 + 9			50.88		6.52		-12.99					155.4	1.3	
	1983	1 4	-8	2445338.5			12.03		48.55		9.70		-10.12					155-2	1-3	
	1983	1 9	• 0	2445343.5			15.69		46.28			9.59			-13-49			154.9		128
_	1983	1 14	•0	2445348.5			19.96	_			17.86				-10.51			151.8		7 162
	1983	1 19	-8	2445353.5			24.78				22.78				-10-53			157.7		103
_	1983	1 24	-0	2445358.5		07 + 9			39.52			9.56			-10-55	_		153.1	2.4	
-	1983	1 29	-0	2445363.5		-	35.90	5		-	34-10				-10-57			145.2	2-5	
	1983	2 3	-8	2445368.5			42-11				40.40				-10.59	-		143-1		103
	1983	2 8	• 3	2445373.5			48.68	5			47-06				-10-51			138-0		7 160
	983	2 13	•0	2445378.5			55.56				54.03				-10.63			132.8		132
	1983	2 18	• 0	2445383.5		34 +10		5			1.25				-13.65			127-6	4.1	
	1983	2 23	.0	2445388-5			13.04	5			3.65				-13.67			155*#	¥.,	
	1983	2 28	-0	2445393.5			17.52				16.20				-13.73			117.2		
	983	3 5	•0	2445398.5	-		25.09	5			23.82				-10.72	and the	. ,	112.1		2 135
1	983	3 10	-0	2445403.5	6 23.2	00 +10	32-73	٤	25.02	6 +10	31.48	9.84	17.35	13.17	-13.74	•4	22.5	107.0	5.*	1 225

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Table 8-2 (contd)

														ă.						
YR	MN	DY	HR	J.D.	R.A.	1950.0	DEC.		R.A.	APPN	DEC.	DELTA	DELDOT	R	RDOT	H,	M ₂	THETA	BETA I	MOON
1933	3	15	-3	2445436.5	6 22.39	9 +10	45.29	5	24.214	+19	37.11	9.89	13.05	10.14	-13.76	.3	22.5	102.0	5.5	58
1983	3	20		2445413.5	5 21.75	5 +10	47.62	5			45.67	9.94	18.48	13.11	-13.78		22.5	55.9	5.6	35
1983	3	25	.3	2445418.5	6 21.30	4 +1D	55.23	5	23.13:	+10	54.13	10.33	18.67	13.33	-17,31	-3	22.5	92.0	5.7	39
1983	3	35	- 9	2445423.5	6 21.02	7 +11	2.48	5	22.853	+11	1.37	10.35	15-64	13.05	-13293	لكرزير	22.5	37.1	5.7	108
1983	4	4	• 3	2445428.5	6 23.92	4 +11	7.53	5	22.75	+11	8.43	13.13	13.41	13.32	-10.85	.3	22.5	52.2	5.7	165
1983	4	9	.3	2445433.5	6 20.99	9 +11	16.35	5	22.816	+11	15.25	10-16	17.95	9.99	-13.87	. 0	22.5	77.4	5.6	125
1983	4	14	- 3	2445436.5	5 21.21	5 +11	22.89	5	23.045	+11	21.73	10.21	17.29	9.75	-13.93	.0	22.5	72.7	5.5	54
1983	4	19	. 3	2445443.5	6 21.50	15 +11	29.13	5	23.432	2 +11	28.00	10.26	16.47	9.92	-10.92	-3,	₹2.5	53.C	5.4	13/0
1983	4		•3	2445448.5	6 22-14	2 +11	35.02	5	23.959	+11	33.57	10.30	15.36	9.57	-10.94			53,4	5.2	76
1983		29	• 0	2445453.5	6 22.82	0 +11	40.55	- 6	24.547	*11	39.37	10.35	14.15	7.85	-10.97	.3	22.5	55.5	5.0	141
1983	5	4	• 0	2445458.5	6 23.63				25.45				12.80		-10.99		22.5	54.2		
1983	5	9	.• D	2445463.5	6 24.55				26.39				11.30		-11.01		22.5	49.9	4.5	94
1983		14	- 0	2445466.5	6 25.51			_	27-447		- 6		9.65		-11.04		22.5	₹5.3	4.2	30
1983		19	• 0	2445473.5	5 26.77				25.507				7.87		-11.36		22.5	41.3	3.9	44
1983		24	• 0	2445478.5	6 28.03			5	29.353			10.50	6.31		-11.38		22.5	35.7		111
1983		29	•0	2445483.5	6 29.37			5	31.20			13.51	4.05		-11.11	_	22.5	32.5		166
1983	5		• 0	2445488.5	6 30.79				32.628			10.52	2.03		-11.13		22.4	25.5		124
1983	5		• 0	2445493.5	6 32.23				34.11			10.52	08		-11.16		55-2	24.4	2.5	63
1983		13	• 0	2445498.5	6 33.83				35.65	-		10.52	-2.25		-11.15		25*3	20.5	2.1	14
1983		18	- 8	2445503.5	6 35.43				37.252			10.51	-4.48		-11.20		22.4	17.9	1.6	ES
1983		23	• 0	2445508.5	6 37.05				38.87				-6.72		-11.23		22.4	13.9		143
1983		28	•0	2445513.5	6 35.72	-			40.55				-5.97		-11.25		22-4	11.7		151
1983	7		•0	2445518.5	6 40.40				42.238				-11.24		-11.28		22.3	10-9	1.2	95
1983	7		•.D	2445523.5	6 42.35				43.92				-13.52		-11.30		22.3	11,7	1.3	
1983		13	-,0	2445523.5	6 43.75			_	45.51				-15.79		-11.33		22.3	13.7	1.5	
1983		18	, ID	2445533.5	6 45.45				47.259				-18.03		-11.36		22.3	15.9		113
1983		23	.0	2445538.5	6 47.10				48.94				-29.22		-11.38		25.2	23.4		167
1983		25	• 0	2445543.5	6 48.72								-22.36		-11.41		22.2	24.2		123
1983	8	2	.0	2445548.5	6 50.29								-24.45		-11.43		22.2	28.2	3.0	
1983	5	7 12	• 0	2445553.5	5 51.81								-26.50		-11.46		22.2	32.3	3.4	
1983 1983			• 0	2445563.5	6 53.27				55-11				-28.46		-11.49		22.1	35.5	3.8	30
1983		17 22	•9	2445568.5	6 54 65				56.489				-30.31 -32.05		-11.51 -11.54		22.1	40.7		144
1983		27	• 0	2445573.5	6 57.13				58.973								22.1	45.0 49.4		150
1983			•0	2445578.5	6 58.21			7			23.13		-33.68 -35.23		-11.57 -11.59		22.0	53.5	4-8 5-2	93 32
1953			•0	2445583.5	5 59.17			7			22:54		-36.58		-11.62		21.9	55.3	5.5	44
1983		11	.0	2445588.5			19.63	7			16.52		-37.81		-11.65		21.9	52.8		114
1983		16	•0	2445593.5			13.81	7			10.96		-38.85		-11.68		21.9	57.4		165
1983		21	•0	2445598.5		7 +11		7		1 +11			-39.73		-11.73		21.8	72.0		128
1983			.0	2445603.5		9 +11		7			59.35		-43.43		-11.73		21.5	3.7	6.3	
1983			.0	2445638.5			55.99	7		-	53,03	7.	-43.95		-11.76		21.7	91.5	6.4	15
1983			•0	2445613.5			50.13	7			47.19		-41.25		-11.79		21.7	86.3	5.5	
1983			.0	2445518.5			44.32	7			41,42		-41.33		-11.82		21.5	91.2		146
1983			.0	2445623.5			38.71	7			35 83		-41.17		-11.85		21.6			146
1983			.0	2445628.5			33.34	7			33.48		-40.78		-11.88			101.1	6.4	68
1983			.0	2445533.5	6 59.70			7			25.42		-40.17		-11.90			105.1	6.3	
1983			-8	2445638.5	6 58.64			7			20+72		-39.32		-11.93			111.2		48
1983			• D	2445643.5	6 57.35				59.21				-38.22		-11.96			115.4		117
1983			-0	2445648.5	6 55.85				57.71				-36.85		-11-99			121.5		164
1983			• 0	2445653.5	6 54.11				55.97			1	-35.25		-12.02			126.9		114
1983			.0	2445558.5	6 52.15				54.02				-33.43		-12.35			132.1	9.7	
1983	11	25	• 0	2445663.5	6 49.99				51.85	_			-31.39		-12.39			137.4	4.5	
1983	11	30	•0	2445668.5	6 47.63	37 +10	5.41	5	49.53	5 +18	3.19	7.63	-29.14		-12.12			142.7	4.1	
1983	12	5	• D	2445673.5	6 45.09				46.95				-26.69		-12.15			148.G	3.6	
1983	12	10	. 0	2445678.5	6 42.38	10 +10	4.45	6	44.25	3 +10	2.38		-24.07		-12.18			153.1	3.1	
1983	12	15	-3	2445583.5	6 39.52	26 +10	5.07	. 6	41.50	1 +18			-21.31	8.33	-12.21			157.9	2.5	
1983	12	20	- 0	2449588.5	6 36.55	54 +10	6.45	5	38.43	1 +10	4.64	7.35	-18.45	9.27	-12.24	•3	21.3	152.2	2.1	19

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YR	NO.	N DY	HR	J.D.	R.A.	950.0	DEC		D. A	APPN	DEC.	DELTA	DELDOT	R	RDOT	- w		THETA	RETA	MOON
									R.A.							<u> </u>	M ₂			
198				2445693.5	6 33.49				35.37				-15.51		-12.27			165.5	1.7	
198		2 30		2445598.5 2445703.5	6 30.35			6	32.24		9.94	7.23	-12.52 -9.50		-12.31 -12.34			155.9		128 158
198		1 9		2445738.5	6 24 - 04			5			15.18	7.20			-12.37			162.8		103
198		1 14	.0	2445713.5	6 20.92			5			23.34	7.19			-12.41			158.6	2.5	
198		1 19		2445718.5	6 17.88			5	1.0		29.14	7.18			-12.44			153.7	3.1	
198		1 24		2445723.5	5 14.89			5			35.53	7.18			-12.47			148.5		103
198		1 29		2445728.5	6 12.05			5			42.46	7.19			-12.51			143.3		163
198		2 3		2445733.5			50.41	6			49.89	7.21			-12.54			137.9		126
198		z a	• 0	2445738.5			58.14	5			57.75	7.23			-12.58			132.5	5.3	
198	1	2 1,3	0	2445743.5	6 4.51	3 +11	6.26	5	6.45	B +11	5.98	7.26		7.90	-12.61			127.1	5.7	
198	4	2 18	.0	2445748.5	6 2.39	4 +11	14.68	6	4.25	0 +11	14.51	730	12.45	7.95	-12.65	.3	20.8	121.7	6.1	72
198		2 23	. 0	2445753.5	6 .49	75 +11	23.37	5	2 + 35	2 +11	23.29	7.33	13.88	7.82	-12.68	.3	20.8	115.4	6.5	142
198	4	2 28	.0	2445758.5	5 58 82	28 +11	32.25	6	7	5 +11	32.25	7.37	15.05	7.79	-12.72	-3	23.8	111.1	6 - 8	149
198		3 4	• 0	2445763.5	5 57.39			5	Ç	5 +11	41.34	7.42	15.95	7.75	-12.75	• D	20.7	105.9	7.1	92
198		3 9		2445768.5	5 56.21			5			50.50	7.47			-12.79	.3	23.7	130.7	7.3	33
198		3 14		2445773.5	5 55.27				51		59.67	7.52			-12.83		20-7	95.6	7.4	
198		3 19			5 54 - 55			5			5.79	7.56			-12.86		20.7	90.5		111
198		3 24	.0	2445783.5	5 54.10			5			17.82	7.61			-12.90	_	23.7			167
198		3 29		2445788.5	5 53.86			5			26.70	7.66			-12.94		29.7	80.5		117
1989		4 3		2445793.5	5 53 85			5			35.40	7.71			-12.98		23.7	75.5	7.4	
198		4 8		2445798.5 2445803.5	5 54 . 05			5			43.86	7.76			-13.31		23.7	71-0	7.3	
1984		4 13		2445808.5	5 54.48 5 55.09			5			52.05 59.91	7.80			-13.05		23.7	56.3	3:1	
198		4 18 4 23		2445813.5	5 55.89			5 5		0 +13		7.84	13.26 11.98		-13.39 -13.13		23.7	51.6 57.0	6.8	
1984		4 28		2445818.5	5 56 - 86			5		-	14.58	7.91			-13.17		20.6	52.5	6.3	144
198		5. 3		2445823.5	5 58.00			5			21.32	7.94	8.95		-13.21		20.5	49.0	5.9	
198		5 8	-	2445828.5	5 59.29			5			27.61	7.96			-13.25	-	23.6	43.6	5.5	-
198		5 13		2445833.5			33.50	5			33.44	7.98			-13.29		20.6	39.3		112
198		5 18		2445838.5			38.92	6			38.79	7.99			-13.33		20.6	35.0		167
1984		5 23	.0	2445843.5	6 3.94	8 +13	43.85	5			43.64	8.33			-13.38		20.6	30.8		115
1984	• 3	5 28	• 0	2445848.5	6 5.72	2 +13	48.26	5	7.53	3 +13	47.97	8.00			-13.42		20.5	26.7	3.7	
1984	(-)	6 2	. Q	2445853.5	5 7.55	8 +13	52.15	5			51.76	7.99	-2.73	7.07	-13.46	.3	23.5	22.7	3.2	14
1984	4 . I	6 7	• 0	2445858.5	6 9.53	3 +13	55.49	6	11.44	6 +13	55.01	7.98	-4.92	7.03	-13.50	. 5	23.5	18.9	2.7	7.8
198		6 12		2445863.5	6 11.54			5			57.70	7.97			-13.55		20.5	15.3	2.2	146
198		6 17		2445868.5	6 13.60	_		5			59.83	7.94			-13.59		20.4	12.2		145
198		6 22		2445873.5	5 15.71			5		4 +14	1.41		-11.65		-13.64		20.4	10.0	1.5	
198		5 27		2445878.5	6 17.85	_		5			2.41		-13.93		-13.68		23.4	9.3	1.4	
198		7 2 7 7		2445883.5	6 20.01			5		7 +14	2.84		-16.21		-13.73		23.3	10.5	1.5	
198		7 7 7 12		2445888.5 2445893.5	6 22.19			5 5		3 +14	2.71		-18.47		-13.77		23.3	13.0		113
198		7 17		2445898.5	6 26.48	_	_	- 6		3 +14	2.02 .79		-29.69		-13.82		23.2	16.2	2.4	
198		7 22		2445903.5	6 28.55			5			59.02		-22.87 -25.02		-13.86 -13.91		23.2	19.8 23.7	3.5	117
178		7 27		2445908.5	6 30.65			5			56.72		-27.13		-13.91		23.1	27.5	3.5 4.1	
198		8 Î		2445913.5	6 32.65						53.92		-29.17		-14.31		23.0	31.7	7.6	
198		8 6		2445918.5	6 34.58			5			50.63		-31.12		-14.36		23.5	35.3		146
198		8 11		2445923.5	6 36.43						46.87		-32.97		-14.11		19.9	40.0	5.7	
198		E 16	. 0	2445928.5	6 38.17	2 +13	44.51				42.69		-34.74		-14.16		19.9	44.2	6.3	
1986) , (8 21	- 0	2445933.5	6 39.79	6 +13	39.99	6	41.72	3 +13	38.09	7.36	-36.41	5.43	-14.21	•3	19.8	45.5	6.8	
1984		8 25		2445938.5	6 41.28			5	43.21	4 +13	33.12	6.95	-37.97		-14.26		19.8	52.9	7.2	
198		8 31		2445943.5	6 42.62			5			27.81		-39.39	5.35	-14.31	.3	19.7	57.3	7.7	114
198		9 5	_	2445948.5	6 43.79			5			22.20		-40.65		-14.35		19.5	51.9	_	166
1984		9 10		2445953.5	6 44.77			6			16.34		-41.77		-14.41		19.5	55.3		116
1984		9 15	•0	2445958.5	6 45.54						10.27		-4272		-14.47		19.5	70.9	€ - 8	
1984		9 20	•0	2445963.5	6 46 . 09				48-02				-43.51		-14.52		19.4	75.5	5-1	
198		9 25	•13	2445968.5	6 46.40			.6 z			57.72		-44.11		-14.58		19.4	80.3	9.3	
198	•	9 30	.0	2445973.5	6 46.44	U +12	23.55		48.5	5 +12	51.34	6+10	-44.49	5.10	-14.63	-3	19.3	85.1	5.4	149

Table B-3. Ephemeris (with Perturbations) for Comet Halley at Daily Intervals from October 5, 1984 to March 23, 1987.

YR MN DY HR	J.D.	R.A. 1950.0 DEC.	R.A.	APPN DEC.	DELTA DELDOT	R RDOT	M ₁ M ₂	THETA	BETA MOON
1984 10 5 .0	2445978.5	6 46.193 +12 47.20	6 48-129	9 +12 44.99	5.97 -44.64	6.05 -14.69	.0 19.	2 90.0	9.5 142
1984 10 6 .0	2445979.5	6 46.107 +12 45.93	6 48.04	4 +12 43-73	5-95 -44-65	6.05 -14.70	.0 19.	2 91.0	9.5 130
1984 10 7 -0	2445980.5	6 46.009 +12 44.67		6 +12 42.47	5.92 -44.64	6-04 -14-71	-0 19-	2 92.0	9.5 119
1984 10 8 -0	2445981.5	6 45.899 +12 43.41		£ +12 41.22	5.89 -44.63	6.03 -14.72	-0 19-		9.5 107
1984 10 9 .0	2445982.5	6 45.776 +12 42.16		3 +12 39.97	5.87 -44.61	6.02 -14.73	-0 19-		9.5 96
1984 10 1G .0	2445983.5	6 45.640 +12 40.91		E +12 38.73	5.84 -44.58	6.01 -14.74	.0 19.		9.5 B4
1984 10 11 •0	2445984.5	6 45.492 +12 39.66		9 +12 37.49	5.82 -44.54	6.00 -14.76	.0 19.		9.5 73
1984 10 12 .0	2445985.5	6 45.330 +12 38.43		E +12 36 a 26	5.79 -44.49	6.00 -14.77	.0 19.		9.5 61
1984 10 13 .0	2445986.5	6 45.155 +12 37.19		3 +12 35 -03	5.77 -44.43	5.99 -14.78	.0 19.		9.5 50
1984 10 14 .0	2445987.5	6 44.966 +12 35.97		5 +12 33 -82	5.74 -44.36	5.98 -14.79	-0 19-		9-5 38
1984 10 15 . 0	2445988.5	6 44.764 +12 34.75		3 +12 32 -61	5.71 -44.28	5.97 -14.80		0 100-1	9.5 27
1984 10 16 • 0 1984 10 17 • 0	2445989.5 2445990.5	6 44.548 +12 33.54 6 44.319 +12 32.34		E +12 31.40	5.69 -44.20	5-96 -14-81	.8 19.		9.4 17
1984 10 18 .0	2445991.5	6 44.075 +12 31.14		E +12 30.21 5 +12 29.03	5.66 -44.10	5.95 -14.83	.0 19.		9.4 14
1984 10 19 .0	2445992.5	6 43.817 +12 29.96		E +12 27-136	5.64 -43.99 5.61 -43.87	5.94 -14.84 5.94 -14.85		0 103.1	9-4 20
1984 10 20 .0	2445993.5	6 43.545 +12 28.79		6 +12 26 70	5.59 -43.74	5.93 -14.86		0 104.2	9.4 31
1984 10 21 .0	2445994.5	6 43.258 +12 27.62		5 +12 25.55	5.56 -43.60	5.92 -14.87		9 106.3	9-3 44 9-3 58
1984 10 22 .0	2445995.5	6 42.957 +12 26.47		8 +12 24-41	5.54 -43.45	5.91 -14.88		9 107.3	9.3 73
1984 10 23 .0	2445996.5	6 42.641 +12 25.33		2 +12 23 29	5.51 -43.29	5.90 -14.90		9 108-4	9.2 87
1984 10 24 .0	2445997.5	6 42.310 +12 24.20		2 +12 22.17	5-49 -43.12	5.89 -14.91		9 109.4	9.2 102
1984 10 25 .0	2445998.5	6 41.964 +12 23.09		6 +12 21.08	5.46 -42.93	5.88 -14.92		9 110.5	9-1 117
1984 10 26 .0	2445999.5	6 41.603 +12 21.99		5 +12 19.99	5.44 -42.74	5.88 -14.93		9 111.5	9.1 131
1984 10 27 .0	2446000.5	6 41.227 +12 20.90		C +12 18-92	5.41 -42.53	5.87 -14.94		9 112.6	9.0 144
1984 10 28 -0	2446001.5	6 40.835 +12 19.83		5 +12 17.86	5.39 -42.31	5.86 -14.96		8 113.7	8-9 156
1984 10 29 .0	2446002.5	6 40.429 +12 18.77	6 42.377	2 +12 16.83	5.36 -42.08	5.85 -14.97		8 114.7	8-9 164
1984 10 30	2446003.5	6 40.006 +12 17.73	6 41.95	C +12 15.81	5.34 -41.84	5.84 -14.98	-0 18-	8 115.8	8.8 163
1984 10 31 .0	2446004.5	6 39.569 +12 16.70	6 41.513	3 +12 14.80	5.32 -41.59	5-83 -14.99	.0 18.	8 110.9	8-7 154
1984 11 1 .0	2446005.5	6 39.115 +12 15.70	6 41.060	C +12 13.82	5-29 -41-33	5.82 -15.00	.0 18.	8 118.0	8.7 143
1984 11 2 .0	2446006.5	6 38.647 +12 14.71		2 +12 12-85	5.27 -41.05	5.81 -15.02	-0 18-	8 119.1	8.6 131
1984 11 3 .0	2446007.5	6 38.162 +12 13.73		8 +12 11-90	5.24 -40.77	5.81 -15.03		7 120.2	8.5 120
1984 11 4 .0	2446008.5	6 37.662 +12 12.78		E +12 10.97	5.22 -40.48	5.80 -15.04		7 121.3	8.4 108
1986 11 5 .0	2446009.5	6 37.146 +12 11.85		2 +12 10.06	5.20 -40.17	5.79 -15.05		7 122.4	8.3 97
1984 11 6 .0	2446010.5	6 36.614 +12 10.93	6 38.56		5.17 -39.86	5.78 -15.06		7 123.5	8.2 85
1984 11 7 .0	2446011.5	6 36.067 +12 10.03	6 38-014		5.15 -39.53	5.77 -15.08		7 124.6	8.1 74
1984 11 8 .0	2446012.5	6 35.504 +12 9.16	6 37-45		5.13 -39.20	5.76 -15.09		7 125.7	8.0 62
1984 11 9 .0 1984 11 10 .0	2446013.5 2446014.5	6 34-925 +12 8.30	6 36.87		5.11 -38.85	5.75 -15.10		8.651 6	7.9 50
1984 11 11 .0	2446015.5	6 34.330 +12 7.47 6 33.719 +12 6.66	6 36.27		5.08 -38.49	5.75 -15.11		6 127.9	7.8 39
1984 11 12 .0	2446016.5	6 33.719 +12 6.66 6 33.092 +12 5.87	6 35.667 6 35.047		5.06 -38.12	5.74 -15.13		6 129.0	7.7 27
1984 11 13 .0	2446017.5	6 32.450 +12 5.10	6 34.399		5.04 -37.75 5.02 -37.36	5.73 -15.14 5.72 -15.15		6 130.1	7-6 18
1984 11 14 .0	2446018.5	6 31.792 +12 4.36	6 33.74		5.00 -36.96	5.71 -15.16		6 131.3 6 132.4	7.5 14 7.4 20
1984 11 15 .0	2446019.5	6 31.117 +12 3.64	6 33.068		4.98 -36.55	5.70 -15.18		5 133.5	7.2 31
1984 11 16 .0	2446020.5	6 30.428 +12 2.94	6 32.378		4.95 -36.13	5.69 -15.19	-	5 134.6	7.1 44
1984 11 17 .0	2446021.5	6 29.722 +12 2.27	6 31.67		4.93 -35.69	5.68 -15.20		5 135.8	7.0 57
1984 11 18 -0	2446022.5	6 29.001 +12 1.62	6 30.95		4.91 -35.25	5.68 -15.21		5 136.9	6.8 71
1984 11 19 .0	2446023.5	6 28.264 +12 1.00		6 +11 59.64	4.89 -34.80	5.6% -15.23		5 138.0	6.7 85
1984 11 20 .0	2446024.5	6 27.512 +12 .40		4 +11 59.08	4.87 -34.33	5.66 -15.24		5 139.2	6.6 100
1984 11 21 .0	2446025.5	6 26.745 +11 59.83		7 +11 58.54	4.85 -33.85	5.65 -15.25		4 140.3	6.4 114
1984 11 22 .0	2446026.5	6 25.962 +11 59.29		5 +11 58-04	4.83 -33.37	5.64 -15.26		4 141.5	6.3 128
1984 11 23 .0	2446027.5	6 25.165 +11 58.77		E +11 37.56	4.81 -32.87	5.63 -15.28		4 142.6	6.1 142
1984 11 24 .0	2446028.5	6 24.352 -11 58.28	6 26.30	6 +11 57.11	4.80 -32.36	5.62 -15.29		4 143.8	6.0 755
1984 11 25 .0	2446029.5	6 23.525 +11 57.82	6 25.480	C +11 56.69	4.78 -31.85	5.61 -15.30	.0 18.	4 144.9	5.8 164
1984 11 26 .0	2446030.5	6 22.684 +11 57.39	6 24.639	9 +11 56.29	4.76 -31.32	5.60 -15.32	.D 18.	4 146.0	5.6 163
1984 11 27 •0	2446031.5	6 21.828 +11 56.98	6 23.783	3 +11 55.93	4.74 -30.78	5.60 -15.33	.0 18.	4 147.2	5.5 154

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YR MN DY	HR	J.D.	R.A. 1950.0 DEC.		R.A.	APPN	DEC.	DELTA	DELDOT	R	RDOT	M,	M,	THETA	BETA	MOON
1984 11 28		2446032.5	6 20.958 +11 56.61		22.914	444	EE 40	/ 72	-30.24	5 50	-15.34		1/10 3	148.3	5 3	142
1984 11 29	•0				22.031				-29-69		-15.36	-0		149.4		131
	-0	2446033.5	6 20.075 +11 56.26	_												
1984 11 30	+0	2446034.5	6 19.178 +11 55.94		21.13				-29-13		-15.37	•0		150.6		119
1984 12 1	-0	2446035.5	6 18.268 +11 55.66		20.22				-28.56		-15-38			151.7		107
1984 12 2	•0	2446036-5	6 17.345 +11 55.40		19.307		- 1		-27.98		-15.39	•0		152.8	4.7	
1984 12 3	-0	2446037.5	6 16.409 +11 55.17	_	18.366				-27.40		-15.41			153.9	4.5	
1984 12 4	-0	2446038.5	6 15.461 +11 54.97		17.418				-26.81		-15.42			155.0	4.3	
1984 12 5	.0	2446039.5	6 14.500 +11 54.81	6	•				-26.21		-15.43			156.1	4.1	
1984 12 6	•0	2446040.5	6 13.529 +11 54.67	ō					-25-61		-15.45	•0		157.2	4-0	
1984 12 7	-0	2446041.5	6 12.545 +11 54.57	_	14.504				-25-00		-15.46	•0		158.3	3.8	
1984 12 8	-0	2446042.5	6 11.551 +73 54.49		13.510				-24-38		-15.47	-0		159,3	3.6	
1984 12 9	- 0	2446043.5	6 10.546 +11 54.45	6	12.50				-23.76		-15.49	-0		160.4	3.5	
1984 12 10	- 0	2446044.5	6 9.531 +11 54.44	6	11.491	+11	53.99	4.54	-23.13		-15.50	-0		161.4	3-3	
1984 12 11	-0	2446045.5	6 8,505 +11 54.46	ć	10.466	+11	54.06	4.52	-22.50	5.47	-15.51	-0	18.2	162.3	3-1	22
1984 12 12	•0	2446046.5	6 7.470 +11 54.51	6	9.437	+11	54.17	4.51	-21.86	5.46	-15.53	-0	18.1	163.3	3.0	
1984 12 13	•0	2446047.5	6 6.426 -11 54.59	6	8.388	+11	54.30	4.50	-21.22	5.45	-15.54	-0	18.1	164.2	2.8	47
1984 12 14	.0	2446048.5	6 5.374 +11 54.70	6	7.33	411	54.47	4.49	-20.57	5.44	-15.55	.0	18.1	165.0	2.7	60
1984 12 15	•0	2446049.5	6 4.313 +11 54.85	6	6.27	+11	54.67	4.48	-19.92	5.44	-15.57	-0	18.1	165.8	2.5	74
1984 12 16	• 0	2446050.5	6 3.244 +11 55.03	6	5.20	E +11	54.90	4.46	-19-26	5-43	-15.58	.0	18.7	166.5	2.4	88
1984 12 17	• D	2446051.5	6 2.167 +11 55.24	6	4.130	+11	55.16	4.45	-18.60	5.42	-15.60	-0	18.1	167.1	2.3	102
1984 12 18	• 0	2446052.5	6 1.084 +11 55.48	6	3.04	+11	55.46	4.44	-17.93	5.41	-15.61	-0	18.1	167.6	2.2	116
1984 12 19	-0	2446053.5	5 59.994 +11 55.76	6	1.958	+11	55.79	4.43	-17.27	5.40	-15.62	.0	18.1	168.1	2.2	130
1984 12 20	•0	2446054.5	5 58.899 +11 56.06	6			56.15		-16.60		-15.64			168.3		143
1984 12 21	-0	2446055.5	5 57.798 +11 56.40	5					-15.92		-15.65			168.5		156
1984 12 22	•0	2446056.5	5 56.692 +11 56.78	5					-15.25		-15.67			168.5		164
1984 12 23	•0	2446057.5	5 55.582 +11 57.18		57.54				-14.57		-15.68			168.4		163
1984 12 24	•0	2446058.5	5 54.468 +11 57.62	Ğ					-13.90		-15.69			168.1		153
1984 12 25	•0	2446059.5	5 53.350 +11 58.09	5				-	-13.22		-15.71			167.7		141
1984 12 26	.0	2446060.5	5 52.230 +11 58.60	5					-12.55		-15.72			167.2		129
1984 12 27	.0	2446061.5	5 51.108 +11 59.14	_	53.07				-11.88		-15.74			166.5		117
1984 12 28	•0	2446062.5	5 49-985 +11 59-71	ś			.24		-11.20		-15.75			165.8	2.6	
1984 12 29	•0	2446063.5	5 48.860 +12 .31		50.827		.90		-10.54		-15.76			165.0	2.7	
1984 12 30		2446064.5	5 47.735 +12 .95		49.707	-	1.59	4.35	-9.87		-15.78			164.2	2.9	
1984 12 31	•0	2446065.5	5 46.611 +12 1.61		48.57		2.31	4.34	-9.21		-15-79			163.3	3.1	
1985 1 1	•0	2446066.5	5 45.486 +12 2.31		47.45		3.07	4.34	-8.55		-15.81			162.3	3-2	_
	•0	2446067.5			46.33		3.86	_	-7·89		-15.82			161.3	3.4	
								4-33		-				160.3		
1985 1 3 1985 1 4	-0	2446068.5	5 43.242 +12 3.81		45.209		4.68 5.53	4.33	-7.24		-15.84			159.2	3.6 3.8	
	•0	2446069.5	5 42.123 +12 4.61					4.32	-6.59		-15.85					
1985 1 5	-0	2446070.5	5 41.007 +12 5.44		42.97		6.42	4.32	-5.95		-15.86			158.1	4.0	
1985 1 6	+0	2446077.5	5 39-894 +12 6-30		41.867		7.33	4.32	-5.31		-15.88			157.0	4.2	
1985 1 7	-0	2446072-5	5 38.785 +12 7.19		40.754	_	8.28	4-31	-4-68		-15.89			155.9	4.4	-
1985 1 8	*0	2446073.5	5 37.681 +12 8.12	_	39.649	_	9.26	4.31	-4.05		-15.91			154.8	4-6	
1985 1 9	-0	2446074.5	5 36.581 +12 9.07	5			–	4.31	-3.43		-15.92			153.6	4.8	
1985 1 10	•0	2446075.5	5 35.487 +12 10.06	5		_		4.31	-2-81		-15.94			152.5	5.0	
1985 1 11	-0	2446076.5	5 34.399 +12 11.08	_	36.368			4.31	-2.21		-15.95			151.3	5.2	
1985 1 12	•0	2446077.5	5 33.317 +12 12.13	5				4.30	-1.60		-15.97			150-2	5-4	
1985 1 13	•0	2446078.5	5 32.242 +12 13.21		34.21			4.30	-1.01		-15.98			149.0		106
1985 1 14	•0	2446079.5	5 31.174 +12 14.32	5				4.30	42		-16-00			147.8		120
1985 1 15	•0	2446080.5	5 30.114 +12 15.46		32.08			4.30	-16		-16.01			146.6		133
1985 1 16	• 0	2446081.5	5 29.063 +12 16.63		31.037			4.30	.73		-16-03			145.4		147
1985 1 17	-0	2446082.5	5 28.020 +12 17.84	5		_		4.30	1.30		-16-04			144.2		159
1985 1 18	•0	2446083.5	5 26.987 +12 19.07	5				4.30	1.85	5.12	-10.06			143.0		166
1985 1 19	•0	2446084.5	5 25.964 +12 20.34	5	27.93	+12	22.07	4.31	2-40	5.12	-10.07	-0	17.8	141.8	6.8	162
1985 1 20	•0	2446085.5	5 24.951 +12 21.63	5	26.920	+12	23.41	4.31	2.34	5.11	-16.09			140.6	7-0	151
1985 1 21	•0	2446086.5	5 23.948 +12 22.96	5	25.918	112	24.79	4.31	3.46		-16.10			139.4		139
1985 1 22	-0	2446087.5	5 22.957 +12 24.32	5	24.927	+12	26.20	4.31	3.98	5.09	-16.12	.0	17.7	138.2	7.4	127
1985 1 23	-0	2446088-5	5 21.977 +12 25.70	5	23.947	1 +12	27.63	4.31	4.48	5.08	-16.13	-5	17.7	137.0	7.6	114

Table B-3 (contd)

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YR	MN DY	HR	J.D.	R.A. 1950.0 DEC.		R.A.	APPN	DEC.	DELTA	DELDOT	R	RDOT	M	M ₂	THETA	BETA	MOON
1985	1 24	-0	2446089.5	5 21.009 +12 27.12	.5	22.975	+12	29.10	4.32	4.97	5.07	-16.15	-0	17.7	135 - 8	7.8	102
1985	1 25	•0	2446090.5	5 20.053 +12 28.56	5	22.023	+12	30.59	4.32	5.45	5.06	-16.16	•0	17.7	134.6	8.0	90
1985	1 26	•0	2446091.5	5 19.130 +12 30.04		21.08C			4.32	5.92	5.05	-16.18	•0	17.7	133.4	8.1	78
1985	1 27	•0	2446092.5	5 18.180 +12 31.54		20.150			4.33	6.38		-16.19	• B	17.7	132.2	8.3	66
1985	1 28	-0	2446093.5	5 17-264 +12 33-07		19.233			4.33	6.82		-15.21	-		131.0	8.5	54
1985 1985	1 29 1 30	.0 .0	2446094.5 2446095.5	5 16.360 +12 34.63		18.330			4-33	7.26		-16.23			129.8	8.7	
1985	1 31	•0	2446096.5	5 15.471 +12 36.22 5 14.596 +12 37.84	_	17-441 16-566			4-34	7.68		-16.24			128.6	8.8	31
1985	2 1	.0	2446097.5	5 13.735 +12 39.48		15.705			4.34	8.09 8.48		-16.26 -16.27			127.4	9.0	
1985	2 5	-0	2446098.5	5 12.889 +12 41.15		14.855			4.35	8.87		-16.29			125.1	9.3	
1985	2 3	.0	2446099.5	5 12.058 +12 42.85		14.028			4.36	9.24		-16.30			123.9	9.5	24
1985	2 4	•0	2446100.5	5 11.241 +12 44.57		13.212			4.36	9.60		-16.32			122.7	9-6	
1985	2 5	•0	2446101.5	5 10.440 +12 46.32	5	12.411	+12	48.82	4.37	9.95		-16.34			121.5	9.8	50
1985	2 6	•0	2446102.5	5 9.655 +12 48.09		11.625			4.38	10.28	4.95	-16.35	•0	17.6	120.3	9.9	65
1985	2 7	.0	2446103.5	5 8.884 +12 49.89		10-855			4.38	10.61		-16-37	-0	17.6	119.2	10.0	
1985	2 8	•0	2446104.5	5 8.130 +12 51.72		10.101			4.39	10.92		-16.38			118.0	10-2	_
1985	2 9	•0	2446105.5	5 7.392 +12 53.57	5	9.362			4.39	11.22		-16.40			116,8	10.3	
1985 1985	2 10	•0	2446106.5	5 6.669 +12 55.45	5	8.640		58.14	4.40	11.50		-16.42			115.7	10.4	
1985	2 11 2 12	•0	2446107.5 2446108.5	5 5.963 +12 57.35 5 5.273 +12 59.27	5 5	7-934		-07	4.41	11.78		-16.43			114.5	10.6	
1985	2 13	•0	2446109.5	5 4.600 +13 1.22	5	7.244 6.57C		2.03	4.41	12.04 12.29		-16.45 -16.47			113.4	10.7	
1985	2 14	•0	2446110.5	5 3.943 +13 3.19	ś	5.914		6.01	4.43	12.53		-16.48			111.1	10.9	
1985	2 15	.0	2446111.5	5 3,303 +13 5,18	5	5.273		8.04	4.44	12.76		-16.50			109.9	11.0	
1985	2 16	•0	2446112.5	5 2.679 +13 7.20	5	4.65C		10.09	4.44	12.97		-16.52			108.8	11,1	
1985	2 17	•0	2446113.5	5 2.073 +13 9.24	5	4.044			4.45	13.17		-16.53			107.7	11.2	
1985	2 18	•0	2446114.5	5 1.483 +13 11.30	5	3.454	+13	14.25	4.46	13.35	4.83	-16.55	-0	17-6	106.5	11.3	
1985	2 19	•0	2446115.5	5 .910 +13 13.39	5	2.831			4.47	13.52	4.82	-16.57	•0	17.6	105.4	11.4	113
1985	2 20	•0	2446116.5	5 .354 +13 15.49	5	2.325			4.47	13.68		-16.58			104.3	11.5	
1985	2 21	•0	2446117.5	4 59.815 +13 17.62	5	1.787			4.48	13.83		-16.60			103.2	11.6	
1985 1985	2 22	•0	2446118.5 2446119.5	4 59.293 +13 19.76	5	1.265			4.49	13.96		-16.62			102.0	11.6	
1985	2 24	.0 .0	2446120.5	4 58.788 +13 21.93 4 58.301 +13 24.12	5			25.01	4.50	14.08		-16.63			100.9	11.7	
1985	2 25	.0	2446121.5	4 57.830 +13 26.32	_	59.801			4.51	14.19 14.29		-16.65 -16.67		17.6 17.6	99.8 98.7	11.8	53 42
1985	2 26	•0	2446122-5	4 57.376 +13 28.55		59.347			4.52	14.37		-16.68		17.5	97.6	11.9	_
1985	2 27	•0	2446123.5	4 56.938 +13 30.79		58.910			4.53	14.44		-16.70		17.5	96.5	12.0	
1985	2 28	•0	2446124.5	4 56.518 +13 33.05		58.485			4.54	14.50		-16.72		17.5	95.4	12.0	
1985	3 1	• 0	2446125.5	4 56.114 +13 35.33		58.086			4.55	14.54		-16.74		17.5	94.4	12.1	13
1985	3 2	•0	2446126.5	4 55.727 +13 37.62	4	57.695	+13	40.85	4.56	14.58	4.72	-16.75	-0	17.5	93.3	12.1	23
1985	3 3	•0	2446127.5	4 55.357 +13 39.93		57.325			4.56	14.60		-16.77		17.5	92.2	12-1	35
1985	3 4	.0	2446128.5	4 55.003 +13 42.25		56.975			4.57	14.61		-16.79		17.5	91.1	12.2	
1985	3 5	•0	2446129.5	4 54.665 +13 44.60		56-638			4.58	14.61		-16.81		17.5	90.1	12.2	
1985 1985	3 7	•0	2446130.5 2446131.5	4 54.344 +13 46.95 4 54.039 +13 49.32		56.317			4-59	14.60		-16.82		17.5	89.0	12.2	
1985	3 8	.0	2446132.5	4 53.749 +13 51.70		56.011 55.722			4.60	14.58		-16.84		17.5	87.9	12-3	
1985	3 9	•0	2446133.5	4 53.476 +13 54.10		55.445			4.61	14.55 14.51		-16.86 -16.88		17.5 17.5	86.9 85.8	12-3	
1985	3 10	.0	2446134.5	4 53.219 +13 56.51		55.192			4.62	14.46		-16.89		17.5	84.8	12.3	
1985	3 11	•0	2446135.5	4 52.977 +13 58.93		54.951		2.30	4.63	14-40		-16.91		17.5	83.8	12.3	
1985	3 12	.0	2446136.5	4 52.752 +14 1.37		54.725		4.74	4.64	14.33		-16.93		17.5	82.7	12.3	
1985	3 13	.0	2446137.5	4 52.541 +14 3.82	4	54-515	+14	7.20	4.65	14.25		-16.95		17-5	81.7	12.3	
1985	3 14	• 0	2446138.5	4 52.347 +14 6.27		54.321		9-67	4-66	14.16		-16-97		17.5	80.7	12.3	
1985	3 15	-0	2446139.5	4 52.167 +14 8.74		54.142			4.66	14-06		-16.98		17.5	79.6	12.3	
1985	3 16	•0	2446140.5	4 52-003 +14 11-22		53.978			4-67	13.95		-17.00		17-5	78-6	12.3	
1985 1985	3 17 3 18	•0	2446141.5	4 51.854 +14 13.71		53-825			4-68	13.83		-17.02		17.5	77.6	12.3	
1985	3 19	•0	2446142.5 2446143.5	4 51.720 +14 16.22 4 51.601 +14 18.72		53.696 53.577			4 - 69	13.70		-17-04		17.4	76.6	12.3	
1985	3 20	*0	2446144.5	4 51.497 +14 21.24		53.473			4.70	13.56 13.40		-17.06		17.4	35.6	12.2	
1985	3 21	.0	2446145.5	4 51.407 +14 23-77		53.383			4.71	13.24		-17.08 -17.09		17.4	74.6 73.6	12.2	
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YR	MN DY	HR	J.D.	R.A. 1950.0 DEC.		R.A. APPN	DEC.	DELTA	DELDOT	R	RDOT	M,	M ₂	THETA	BETA	MOON
1985	3 22	•0	2446146.5	4 51.332 +14 26.30		53.30E +14	29.75	4.72	13.07	5.52	-17.11	.0	17.4	72.6	12.1	67
1985	3 23	.0	2446147.5	4 51.272 +14 28.85	4	53.248 +14		4.73	12.89		-17.13		17.4	71.6	12.1	55
1985	3 24	.0	2446148.5	4 51.225 +14 31.39		53.201 +14		4.73	12.71		-17.15		17.4	70.6	12.1	44
1985	3 25	•0	2446149.5	4 51.192 +14 33.95		53-165 +14	**	4.74	12.51		-17.17		17.4	69.6	12.0	32
1985	3 26	.0	2446150.5	4 51.173 +14 36.51	4	53.15C +14		4.75	12.30		-17.19		17.4	68.6	12.0	21
1985	3 27	•0	2446151.5	4 51-168 +14 39-07	4	53-146 +14		4.76	12.09		-17.21		17.4	67.6	11.9	12
1985	3 28	.0	2446152.5	4 51.177 +14 41.64	4	53.155 +14	45.09	4.76	11.86		-17.23	.0	17.4	66.7	11.9	10
1985	3 29	.0	2446153.5	4 51.198 +14 44.22	4	53.177 +14	47.67	4.77	11.63	4.45	-17.24	.0	17.4	65.7	11.8	19
1985	3 30	.0	2446154.5	4 51.233 +14 46.80	4	53.212 +14	50.24	4.78	11.39	4.44	-17.26	-0	17.4	64.7	11.7	31
1985	3 31	.0	2446155.5	4 51.281 +14 49.38	4	53.260 +14	52-82	4.78	11.15	4.43	-17.28	-0	17.4	63.8	11.7	43
1985	4 1	-0	2446156.5	4 51.342 +14 51.96	4	53.322 +14	55.40	4.79	10.90	4.42	-17.30	-0	17.4	62.8	11.6	56
1985	4 2	•0	2446157.5	4 51.415 +14 54.55	4	53.396 +14	57.99	4.80	10.64	4.41	-17.32	-0	17.4	61.8	11.5	70
1985	4 3	•0	2446158.5	4 51.501 +14 57.13	4	53.482 +15	-57	4-80	10.37	4-40	-17.34	-0	17-3	60.9	11.4	84
1985	4 4	•0	2446159.5	4 51.600 +14 59.72	4	53.580 +15	3.16	4.81	10.13	4.39	-17.36	.0	17.3	59=9	11.4	99
1985	4 5	-0	2446160.5	4 51.710 +15 2.31	4	53.691 +15		4.81	9.82	4.38	-17.38	-0	17.3	59.0	11.3	114
1985	4 6	•0	2446161.5	4 51.833 +15 4.90	4	53.814 +15		4.82	9.53		-17.40	.0	17.3	58.1	11.2	
1985	4 7	-0	2446162.5	4 51.967 +15 7.49	4	53.945 +15	10.91	4.82	9.24	4.36	-17.42		17.3	57.1	11.1	143
1985	4 8	-0	2446163.5	4 52.113 +15 10.08	4	54.095 +15	13.49	4.83	8.95	4.35	-17.44	-0	17.3	56.2	11.0	157
1985	4 9	.0	2446164.5	4 52.271 -15 12.67	4	54.253 +15	16-07	4.83	8.64	4.34	-17.46	-0	17.3	55.3	10.9	
1985	4 10	.0	2446165.5	4 52.440 +15 15.26	4	54.423 +15	18.65	4.84	8.33	4.33	-17.48	-0	17.3	54.3	10.8	167
1985	4 11	.0	2446166.5	4 52.620 +15 17.85	4	54.604 +15	21.23	4.84	8.02	4.32	-17.50	•0	17.3	53.4	10-7	155
1985	4 12	• 0	2446167.5	4 52.812 +15 20.44	4	54.797 +15	23.81	4.85	7.70	4.31	-17.52	.0	17.3	52.5	10.6	143
1985	4 13	• 0	2446168.5	4 53.015 +15 23.02	4	55.00C +15	26.39	4.85	7.37	4-30	-17.54	-0	17.3	51.6	10.5	130
1985	4 14	-0	2446169.5	4 53.229 +15 25.61	4	55.214 +15	28.96	4.86	7.04	4.29	-17.56	.0	17.3	50.7	10.4	118
1985	4 15	•0	2446170.5	4 53.453 +15 28.19	4	55.435 +15		4.86	6-70		-17.58		17.2	49.7	10.3	106
1985	4 16	-0	2446171.5	4 53.688 +15 30.76	4			4-86	6.35	4-27	-17.60		17.2	48.8	10.2	94
1985	4 17	-0	2446172.5	4 53.934 +15 33.34	4	55.921 +15	36.66	4.87	6.00	4.26	-17.62	.0	17.2	47.9	10.1	82
1985	4 18	-0	2446173.5	4 54.190 +15 35.91	4	56.177 +15	39.22	4.87	5.64	4.25	-17.64	-0	17.2	47.0	10.0	70
1985	4 19	•0	2446174.5	4 54.456 +15 38.47	4	56.444 +15	41.77	4.87	5.28	4.24	-17.66	-0	17.2	46.1	9.8	59
1985	4 20	.0	2446175.5	4 54.732 +15 41.03	4	56.72C +15	44.31	4.88	4.91	4.23	-17.68	-0	17.2	45.2	9.7	47
1985	4 21	-0	2446176.5	4 55.018 +15 43.58	4	57.007 +15	46.85	4.88	4.54	4.22	-17.70	.0	17.2	44.3	9.6	36
1985	4 22	-0	2446177.5	4 55.314 +15 46.13	4	57.303 +15	49.39	4.88	4.16	4.21	-17.73	-0	17.2	43.4	9.4	25
1985	4 23	•0	2446178.5	4 55.619 +15 48.68	4	57.605 +15	51.92	4.89	3.77	4.20	-17.75	.0	17.2	42.6	9-3	14
1985	4 24	.0	2446179.5	4 55.934 +15 51.21	4	57.924 +15	54.44	4.89	3.39	4.19	-17.77	-0	17.2	41.7	9.2	9
1985	4 25	•0	2446180.5	4 56.258 +15 53.74	4	58.245 +15	56.95	4.89	2.99	4.18	-17.79	-0	17.2	40.8	9.0	15
1985	4 26	• •0	2446181-5	4 56.590 +15 56.26	4	58.582 +15	59.46	4.89	2.60	4.17	-17.81	-0	17.1	39.9	8.9	26
1985	4 27	.0	2446182.5	4 56.932 +15 58.78	4	58.925 +16	1.96	4.89	2.20	4.16	-17.83	•0	17.1	39.0	E.8	38
1985	4 28	•0	2446183.5	4 57.283 +16 1.28	4	59.276 +16	4.45	4.89	1,79	4.15	-17.85	-0	17.1	38.2	8.6	5 C
1985	4 29	• 0	2446184.5	4 57.642 +16 3.78	4	59.636 +16	6.93	4.89	1.39	4.14	-17.87	-0	17.1	37.3	8.5	63
1985	4 30	•0	2446185.5	4 58.010 +16 6.27	5	.004 +16	9.40	4.89	-98	4.13	-17.90	.0	17.1	36.4	8.3	77
1985	5 1	.0	2446186.5	4 58.386 +16 8.75	5	.38C +16	11.86	4.90	•5€	4.12	-17.92	-0	17.1	35.6	8.2	91
1985	5 2	-0	2446187.5	4 58.770 +16 11.22	5	.765 +16	14.31	4.90	-15	4.11	-17.94	.0	17.1	34.7	8.0	105
1985	5 3	-0	2446188.5	4 59.162 +16 13.68	5	1.158 +16	16.76	4.90	27	4.10	-17.96		17.1	33.8	7.9	120
1985	5 4	•0	2446189.5	4 59.562 +16 16.13	5	1.558 +16	19.19	4.90	69	4.09	-17.98	-0	37.1	33.0	7.7	135
1985	5 5	•0	2446190.5	4 59.969 +16 18.57	5	1.967 +16	21.61	4.89	-1.12	4.08	-18.01	.0	17.1	32.1	7.6	149
1985	5 6	-0	2446191.5	5 .385 +16 21-01	5	2.383 +16	24.02	4.89	-1.54	4.07	-18.03	-0	17.0	31.3	7.4	163
1985	5 7	•0	2446192.5	5 .808 +16 23.43	5	2.806 +16	26.42	4.89	-1.97	4.06	-18.05	-0	17.0	30.4	7.2	171
1985	5 8	•0	2446193.5	5 1.238 +16 25.83	5	3.237 +16	28.81	4.89	-2.40	4.04	-18.07	.0	17.0	29.6	7.1	162
1985	5 9	•0	2446194.5	5 1.676 +16 28.23	5	3.676 +16	31.18	4.89	-2.84	4.03	-18.09	-0	17.0	28.7	6.9	149
1985	5 10	•0	2446195.5	5 2.120 +16 30.62	5	4.121 +16	33.55	4.89	-3.28		-18.12	-0	17.0	27.9	6.7	137
1985	5 11	•0	2446196.5	5 2.572 +16 33.00	5	4.574 +16	35.90	4.89	-3.72	4.01	-18.14	.0	17.0	27.1	6.6	124
1985	5 12	•0	2446197.5	5 3.031 +16 35.36	5	5.034 +16	38.25	4.88	-4.16	4.00	-18.16	•C	17.0	26.2	6.4	112
1985	5 13	•0	2446198.5	5 3.497 +16 37.71	5	5.50C +16	40.58	4.88	-4.61	3.99	-18.18	-0	17.0	25.4	6-2	100
1985	5 14	.0	2446199.5	5 3.969 +16 40.05	5	5.973 +16	42.89	4.88	-5.06	3.98	-18.21	-0	16.9	24.6	6-1	
1985	5 15	-0	2446200-5	5 4.448 +16 42.38	5	6.453 +16	45.20	4.88	-5.51	3.97	-18.23	-0	16.9	23.8	5.9	
1985	5 16	•0	2446201.5	5 4.934 +16 44.69	5	6.935 +16	47.48	4.87	-5.96	3.96	-18.25	.0	16.9	22.9	5.7	
1985	5 17	•0	2446202-5	5 5.426 +16 46.99	5	7.431 +16	49.76	4.87	-6.42		-18.28	-0	16.9		5.5	
												_	-			

Table B-3 (contd)

YR	MN DY	HR	J.D.	R.A. 1950.0 DEC.		R.A. APPN	DEC.	DELTA DI	ELDOT	R	RDOT	M,	М,	THETA	BETA	MOON
1985	5 18	• 0	2446203.5	5 5.924 +16 49.28	5	7-930 +16	52.02	4.87 -	-6.88	3.94	-18.30	-0	16.9	21.3	5.4	41
1985	5 19	• 0	2446204.5	5 6.428 +16 51.55	5	8.435 +16			-7.34		-18.32		16.9	20.5	5.2	30
1985	5 20	•0	2446205.5	5 6.938 +16 53.81	5	8.945 +16			-7.81		-18.35		16.9	19.7	5-C	19
1985	5 21	-0	2446206.5	5 7.453 +16 56.05	5	9.462 +16	58.72		-8.27		-18.37		16-8	18.9	4.8	10
1985	5 22	-0	2446207.5	5 7.975 +16 58.28	5	9.984 +17	-93		-8.74		-18.39		16.8	18.1	4.6	10
1985	5 23	•0	2446208.5	5 8.502 +17 .49	5	10.512 +17	3.11	4.84 -	-9.21	3.89	-18.42	-0	16.8	17.3	4.4	20
1985	5 24	•0	2446209.5	5 9.034 +17 2.69	5	11.045 +17	5.29	4.84	-9-68	3.88	-18-44	-0	16.8	16.5	4.3	32
1985	5 25	.0	2446210.5	5 9.572 +17 4.88	5	11.584 +17	7.45	4.83 -1		3.87	-18.47	•0	16.8	15.7	4.1	44
1985	5 26	•0	2446211.5	5 10-115 +17 7-05	5	12.127 +17	9.59	4.82 -1			-18.49	•0	16.8	15.0	3.9	57
1985	5 27	•0	2446212.5	5 10.663 +17 9.20		12.676 +17	- ,	4.82 -1			-18.51		16.8	14.2	3.7	70
1985	5 28	-0	2446213.5	5 11.215 +17 11.33	-			4.81 -1			-18.54		16.7	13.4	3.5	83
1985	5 29	•0	2446214.5	5 11.773 +17 13.45		13.787 +17		4.81 -1			-18.56		16.7	12.7	3.3	97
1985	5 30	•0	2446215.5	5 12.335 +17 15.56		14.350 +17		4.80 -1			-18.59		16.7	12.0		111
1985	5 31	•0	2446216.5	5 12.901 +17 17.65		14.917 +17		4.79 -1			-18.61		16.7	11.2		125
1985	6 1	-0	2446217.5	5 13.472 +17 19.72	-	15.485 +17		4.78 -1			-18.64		16.7	10-5		140
1985	6 2	-0	2446218.5	5 14.047 +17 21.77				4.78 -1			-18.66		16.7	9.8		154
1985	6 3	•0	2446219.5	5 14.627 +17 23.81 5 15.211 +17 25.83	5	16.645 417		4.77 -1			-18.69		16.7	9-2		167
1985	6 4	•0 •0	2446221.5	5 15.798 +17 27.83		17.23C +17		4.76 -1 4.75 -1			-18.71 -18.74		16.6	8.5 7.9		170 158
1985	6 6	•0	2446222.5	5 16.390 +17 29.82	-			4.74 -1			-18.76	.0		7.3		145
1985	6 7	•0	2446223.5	5 16.985 +17 31.79		19.007 +17		4.73 -1			-18.79		16.6	6.8		132
1985	6 8	.0	2446224.5	5 17.584 +17 33.74				4.72 -1			-18.81	.0	16.6	6.4		119
1985	6 9	-0	2446225.5	5 18.187 +17 35.68				4.71 -1			-18.84			6.0	1.6	
1985	6 10	•0	2446226.5	5 18.793 +17 37.60				4.70 -1			-18.86		16.5	5.7	1.6	95
1985	6 11	.0	2446227.5	5 19.403 +17 39.50	Š	21.428 +17		4.69 -1			-18.89		16.5	5.5	1.5	83
1985	6 12	•0	2446228.5	5 20.016 +17 41.38	5	22.042 +17		4-68 -1			-18-92		16.5	5.4	1.5	71
1985	6 13	-0	2446229.5	5 20.633 +17 43.25	5	22.659 +17	45.28	4.67 -1	19-16	3.66	-18.94		16.5	5.5	1.5	60
1985	6 14	•0	2446230.5	5 21.252 +17 45.09	5	23.275 +17	47.10	4.66 -1	19.64 .	3.65	-18-97	-0	16.5	5-6	1.6	48
1985	6 15	-0:	2446231.5	5 21.874 +17 46.92	5	23.902 +17	48.89	4.65 -2	20.12	3.64	-18.99	-0	16.4	5.9	1-6	37
1985	6 16	-0	2446232.5	5 22.500 +17 48.73		24.528 +17		4.64 -7		3.63	-19.03	-0		6.3	1.7	26
1985	6 17	•0	2446233.5	5 23.127 +17 50.53				4.62 -2	21.07		-19-05	-0	16.4	6.7	1.9	15
1985	6 18	•0	2446234.5	5 23.758 +17 52.30		25.788 +17		4-61 -2			-19.07	•0	16.4	7.2	2.0	.8
1985	6 19	· ∙0	2446235.5	5 24.391 +17 54.06		26-422 +17		4-60 -2			-19-10		16.4	7.7	2.2	14
1985	6.25	-0	2446236.5	5 25.026 +17 55.79	5	27-058 +17		4.59 -2			-19.13		16.3	8.3	2.4	25
1985	6 21	•0	2446237.5	5 25.664 +17 57.51		27.697 +17		4.57 -2			-19.16		16.3	9-0	2.5	37
1985	6 22	•0	2446238.5	5 26.303 +17 59.21		28.337 +18	-96	4.56 -2			-19-18		16.3	9.6	2.7	50
1985	6 23	•0	2446239.5	5 26.945 +18 .89		28.975 +18	2.61	4.55 -2			-19.21		16-3	10.3	2.9	63
1985	6 24	-0	2446240.5	5 27.588 +18 2.55 5 28.233 +18 4.19		29.623 +18	4.24	4.53 -2			-15.24		16.3	11.0	3.1	76
1985 1985	6 25 6 26	•0 •0	2446242.5	5 28.860 +18 5.82	_	30.269 +18	5.86 7.45	4.52 -2 4.30 -2			-19.26 -19.29		16.2	11.7	3.3	90 103
1985	6 27	.0	2446243.5	5 29.528 +18 7.42		31.565 +18	9.02	4.49 -2			-19.32		16.2	13.1		117
1985	6 28	.0	2446244.5	5 30.177 +18 9.01	5	32.215 +18		4.47 -2			-19.35	_		13.8	-	131
1985	6 29	-0	2446245.5	5 30.828 +18 10.58	5	32.867 +18		4.46 -2			-19.38	-0	16.2	14.6		145
1985	6 30	•0	2446246.5	5 31.480 +18 12.13				4.44 -2			-19-41		16.1	15.3		159
1985	7 1	.0	2446247.5	5 32.133 +18 13.66	-	34.173 +18		4.43 -2			-19.43	.0	16.1	16.1		170
1985	7 2	-0	2446248.5	5 32.787 +18 15.17	5	34.828 +18		4.41 -2			-19.46	.0	16.1	16.8		167
1985	7 3	•0	2446249.5	5 33.441 +18 16.67	-			4.39 -2			-19.49	.0		17.6		155
1985	7 4	-0	2446250.5	5 34.097 +18 18.14	5	36.14C +18		4.38 -2			-19.52	.0		18.3		142
1985	7 5	-0	2446251.5	5 34.753 +18 19.60	5	36.797 418		4.36 -2			-19.55	-0		19.1		129
1985	7 6	.0	2446252.5	5 35.410 +18 21.04	5	37.454 +18	22.35	4.34 -2	29.92	3.40	-19.58	.0	16.0	19.9	5.8	116
1985	7 7	-0	2446253.5	5 36.067 +18 22.47	5	38-117 +18		4.33 -3			-19.61	-0		20.6		103
1985	7 8	•0	2446254.5	5 36.724 +18 23.87	5	38.770 +18		4.31 -3			-19.64	-0		21.4	6.3	
1985	7 9	-0	2446255.5	5 37.382 +18 25.26		39.428 +18		4.29 -3			-19-67		15.9	22.2	6.5	80
1985	7 10	•0	2446256.5	5 38.040 +18 26.63		40.087 +18					-19.70		15.9	22.9	6.8	68
1985	7 11	-0	2446257.5	5 38.697 +18 27.98		40.745 +18					-19.73		15.9	23.7	7.0	
1985	7 12	-0	2446258.5	5 39.355 +18 29.31		41.403 +18		4.23 -3			-19.76			24-5	7-3	45
1985	7 13	•0	2446259.5	5 40.012 +18 30.63	>	42.061 +18	31-17	4.22 -3	23.02	3.32	-19.79	12.0	12.8	25.3	7.5	33

YR	MN	DY	HR	J.D _r	R.A.	1950.0	DEC.		R.A.	APPN	DEC.	DELTA	DELDOT	R	RDOT	M	M ₂	THETA	BETA	MOON
1985	7	14	-0	2446260.5	5 40.6	69 +78	31.93	5	42.719	+18	32.97	4.20	-33.49	3.31	-19.82	14.9	15.8	26.0	7.7	55
1985	7	15	.0	2446261.5	5 41.3	25 +18	33.21	5	43.375	+18	34.22	4.18	-33.93	3.30	-19.85	14.9	15.8	26.8	8.0	12
1985	7	16	• 0	2446262.5	5 41.9	80 +18	34.47	5	44.031	418	35.45	4.16	-34.37	3.29	-19.88	14.9	15.8	27.6	8.2	8
1985	7	17	-0	2446263.5	5 42.6	34 +18	35.72	5	44.687	+18	36.67	4.14	-34.80	3.28	-19.91	14.8	15.7	28.4	8.5	17
1985			-0	2446264.5		87 +18		5	45-341				-35.23					29.2	8.7	
1985			•0	2446265.5		39 +18		5	45.993				-35.66		-19.97			30.0	9.0	
1985			• 0	2446266.5		90 +18			46.645				-36.09		-20-00			30.7	9.2	
1985			•0	2446267.5		39 +18			47.294				-36.51		-20.03			31.5	9.5	
1985	7	22	-0	2446268.5	5 45.8	86 +18	41.71	5	47.942	+18	42.50	4.03	-36.93	3.22	-20.06	14.7	15.6	32.3	9.7	82
1985			•0	2446269.5		31 +18			48.588				-37.35		-20.10			33.1	10.0	
1985	-		-0	2446270.5	5 47.1	74 +18	43.99		49.231				-37.76	3.20	-20.13	14.6	15.6	33.9	10.2	110
1985			•0	2446271.5		15 +18			49.873				-38.17		-20-16			34.7	10.5	
1985			.0	2446272.5	5 48-4	54 +18	46.21		50.512				-38.57		-20.19			35.5	10.7	137
1985			.0	2446273.5		90 +18			51.149				-38-98		-20.22			36.3	10-9	
1985			-0	2446274.5	5 49.7	23 +18	48.38	5	51.783	+18	48.97	3.90	-39.38	3.15	-20-26	14.5	15.4	37.1	11.2	164
1985			-0	2446275.5		53 +18			52.414				-39.77		-20-29			37.9	11.4	
1985		30	•0	2446276.5	5 50.9	81 +18	50,49		53.043			3.86	-40.16	3.13	-20-32	14.4	15.4	38.7	11.7	163
1985		31	-0	2446277.5		05 +18			53.668				-40.55		-20.36			39.5	11.9	
1985		1	-0	2446278.5		27 +18		_	54-290				-40.94		-20.39			40.3	12.2	
1985		2	-0	2446279.5		44 +18			54.908				-41.32		-20.42			41.1	12.4	
1985		3	•0	2446280-5		58 +18			55.523				-41.71		-50.44			41.9	12.7	
1985	-	-4	•0	2446281.5		69 +18			56-134				-42.08		-20.49			42.7	12.9	
1985		5	• 0	2446282.5		75 +18			56.741				-42.46		-20.52			43.5	13.2	
1985	_	6	-0	2446283-5		77 +18			57.344				-42-83		-20.56			44.3	13.4	
1985		7	-0	2446284.5		75 +18			57.947				-43.20		-20-59			45.1	13.7	64
1985		8	-0	2446285.5		68 +18		-	58.536	-			-43.57		-20.63			45.9	13.9	
1985		9	•0	2446286.5		56 +19	-32		59.124		-55		-43.93		-20.66			46.7	14.2	
1985	_	10	•0	2446287.5		39 +19	1.25		59.708		1.44		-44.29		-20.70			47.5	14.4	
1985			•0	2446288+5		17 +19	2.17	6		+19	2.33		-44.65		-20.73			48.4	14.7	
1985			-0	2446289.5		90 +19	3.08	- 6		+19	3.22		-45.00		-20.77			44.2	14.9	
1985			•0	2446290.5		56 +19	3.98	6	1.427		4.09		-45.35		-20.80			50.0	15.2	
1985			•0	2446291.5		16 >19	4.88	ð	1.988		4.96		-45.69		-20.84			50.8	15.4	
1985			-0	2446292.5		70 +19	5.77	6	2.543		5.82		-46.03		-20-87			51.6	15.7	-
1985			•0	2446293.5		17 +19	6.65	6	3.091		6.68		-46.37		-20.91			52.5	15.9	47
1985			•0	2446294.5		58 +19	7.53	6	3.637		7.53		-46.70		-20.95			53.3	16.2	60
1985	_		•0	2446295.5		91 +19		6	4.165	+19	8.38		-47.03		-20.98			54.1	16-4	74
1985			•0	2446296.5		16 +19		6	4-691		9.23		-47.35		-21.02			55.0	16.7	
1985			•0	2446297.5		33 +19		ő			10.08		-47.67		-21.06		-	55.8	16.9	102
1985		21	-0	2446298.5		43 +19		ó			10.92		-47.98		-21.09			56.6	17.2	117
1985			•0	2446299.5		43 +19		6	6.220	+19	11.76		-48.28	2.85	-21.13	13.5	14.6	57.5	17.4	131
1985			•0	2446300.5		35 +19		6	6.713	+19	12.60		-48.58	2.84	-21.17	13.5	14.6	58.3	17.6	144
1985			-0	2446301.5	6 5.1	18 +19	13.62	6	7.196	+19	13.44	3.21	-48.88	2.83	-21.21	13.4	14.5	59.2	17.9	158
1985		25	•0	2446302.5		91 +19		6			14.29		-49.17		-21.25			60.0	18.1	169
1985	8	26	-0	2446303.5	6 6.0	54 +19	15.37	6	8.134	+19	15.14	3.15	-49.40	2.80	-21.28	13.4	14.5	60.9	18.4	169
1985			• 0	2446304.5		08 +19		6	8.588	+19	16.00	3.12	-49.74	2.79	-2:.32	13.3	14.4	61.7	18.6	158
1985		28	•0	2446305.5		50 +19		6			16.86	3.10	-50-01	2.78	-21.36	13.3	14.4	62.6	18.8	145
1985		29	•0	2446306.5		82 +19		6	9.464	+19	17.72		-50.28	2.77	-21-40	13.2	14.4	63.4	19.1	132
1985		30	-0	2446207.5		03 +19		6	9.886	+19	18.60	3.04	-50.55	2.75	-21.44	13.2	14.3	64.3	19.3	120
1985	-	31	• 0	2446308.5		12 +19		6	10.295			3.01	-50.81		-21.48			65.2	19.5	107
1985		1	•0	2446309.5		08 +19			10.692		1. 1	2.98	-51.07	2.73	-21.52	13.7	14.2	66.0	19.7	95
1985		2	-0	2446310.5		92 +19		- 6	11.077	+19	21.28	2.95	-51.32	2.72	-21.56	13.0	14.2	66.9	20.0	23
1985		3	•0	2446311.5		63 +19			11.448				-51.57		-21.60			67.8	20.2	71
1985		4	-0	2446312.5		20 +19			11.806			2.89	-51.81	2.69	-21.64	12.9	14.1	68.7	20.4	69
1985		5	-0	2446313.5		64 +19			12.150			2.86	-52.05	2.68	-21.68	12.9	14.1	69.6	20.6	48
1985		6	.0	2446314.5	6 10.3	92 +19	25.47	6	12.479	+19	25.02	2.83	-52.28	2.67	-21.72	12.8	14-0	70.5	20.9	37
1985		7	•0	2446315.5		05 +19			12.793			2+80	-52.51	2.65	-21.76	12.8	14.0	71.3	21.1	25
1985	9 .	8	•0	2446316.5	6 11.0	02 +19	27.47	6	13.091	+19	27.00	2.77	-52.73	2-64	-21.80	12.7	13.9	72.2	21.3	14

OF POOR QUALITY

Table B-3 (contd)

			12-15											
YR MN DY	HR	J.D.	R.A. 1950.0 DEC.	R.A.	APPN	DEC.	DELTA DELDOT	R	RDOT	M,	м ₂	THETA	BETA I	MOON
1985 9 9	-0	2446317.5	6 11.283 +19 28.50	6 13.37	72 +19	28.01	2.74 -52.94	2.63	-21.84	12.7	13.9	73.1	21.5	8
1985 9 10	•0	2446318.5	6 11.546 +19 29.55	6 13-63	SE +19	29.05	2.71 -53.15		-21.88			74.1	21.7	14
1785 9 11	.0	2446319.5	6 11.791 +19 30.63	6 13-88	33 +19	30.11	2.68 -53.36	2.60	-21.93	12.6	13.8	75.0	21.9	26
1985 9 12	-0	2446320.5	6 12.018 +19 31.73	6 14.11	16 +19	31 420	2.65 -53.55	2.59	-21.97	12.5	13.7	75.9	22.1	39
1985 9 13	-0	2446321.5	6 12.225 +19 32.85	6 14.31	18 +19	32 , 31	2.62 -53.74	2.58	-22-01	12.5	13.7	76.8	22.3	52
1985 9 14	-0	2446322.5	6 12.412 +19 34.00	6 14.50	16 +19	33.46	2.58 -53.92	2.57	-22-05	12.4	13.7	77.7	22.5	66
1985 9 15	•0	2446323.5	6 12.578 +19 35.19	6 14-67	72 +19	34 463	2.55 -54.09	2.55	-22-10	12.4	13.6	78.7	22.7	81
1985 9 16	-0	2446324.5	6 12.722 +19 36.40			35 84	2.52 -54.26		-22-14			79.6	22.9	95
1985 9 17	-0	2446325.5	6 12-842 +19 37-65			37.08	2.49 -54.42		-22.18			80.5	23.1	
1985 9 18	-0	2446326.5	6 12.939 +19 38.93	6 15.03			2.46 -54.57		-55-53			81.5	23.3	
1985 9 19	•0	2446327.5	6 13.012 +19 40.25	6 15-10			2.43 -54.71		-22.27			82.5	23.5	
1985 9 20	•0	2446328.5	6 13.058 +19 41.61		-	41,03	2.40 -54.85		-22.31			83.4	23-6	
1985 9 21	•0	2446329.5	6 13.078 +19 43.02			42,43	2.36 -54.97		-22-36			84.4	23.8	
1985 9 22	-0	2446330.5	6 13.069 +19 44.47	6 15.16			2.33 -55.09		-22.40			85.4	24.0	
1985 9 23	•0	2446331.5	6 13.031 +19 45.97			45,38	2.30 -55.20		-22-45			86.4	24.1	
1985 9 24	•0	2446332.5	6 12.964 +19 47.52			46,94	2.27 -55.30		-22.49			87.4	24.3	
1985 9 25 1985 9 26	-0	2446333.5	6 12.864 +19 49.12			48,54	2.24 -55.40		-22.54			88.4	24.4	
1985 9 27	•0	2446334.5	6 12.731 +19 50.77 6 12.564 +19 52.49	6 14-83			2.20 -55.48 2.17 -55.56		-22.58			89.4	24.6	
1985 9 28	.0	2446336.5	6 12.361 +19 54.26	6 14.46			2.14 -55.63		-22.63			90.4	24.7	
1985 9 29	.0	2446337.5	6 12-121 +19 56-10			55.56	2.11 -55.69		-22.68 -22.72			91.4	24.8	87
1985 9 30	.0	2446338.5	6 11.841 +19 58.00	6 13.94			1.08 -55.74		-22.77			93.5	25.1	75
1985 10 1	.0	2446339.5	6 11.520 +19 59.98	6 13.67			2.04 -55.78		-22.82			94.5	25.2	63
1985 10 2	.0	2446340.5	6 11.155 +20 2.02	6 13.26			2.01 -55.82		-22.87			95.6	25.3	52
1985 10 3	.0	2446341.5	6 10.746 +20 4.14		57 +20		1.98 -55.84		-22.91			96.7	25.4	40
1985 10 4	.0	2446342.5	6 10.288 +20 6.34	6 12.40			1.95 -55.85		-22.96			97.8	25.4	28
1985 10 5	.0	2446343.5	6 9.782 +20 8.62	6 11.89			1.91 -55.85		-23.01			98.9	25.5	17
1985 10 6	.0	2446344.5	6 9.222 +20 10.98			10.59	1.88 -55.84		-23.06				25.6	8
1985 10 7	-0	2446345.5	6 8.608 +20 13.43			13.07	1.85 -55.81		-23.11				25.6	13
1985 10 8	-0	2446346.5	6 7.936 +20 15.98	6 10-0	4 +20	15.65	1.82 -55.77	2.25	-23-16	10-9	12.3	102-3	25.7	22
1985 10 9	-0	2446347-5	6 7.203 +20 18.61	6 9.37	22 +20	18.33	1.79 -55.72	2.24	-23.20	10.8	12.3	103-4	25.7	35
1985 10 10	.0	2446348.5	6 6.406 +20 21.35	6 8.57	26 +20	21.10	1.75 -55.66	2.23	-23.25	10.8	12.2	104.6	25.7	48
1985 10 11	•0	2446349.5	6 5.541 +20 24.18	6 7.66	0S+ E8	23.98	1.72 -55.58	2.21	-23.30	10.7	12.1	105.8	25.7	62
1985 10 12	-0	2446350.5	6 4.605 +20 27.11			26.96	1.69 -55.49		-23.35				25.7	76
1985 1G 13	•0	2446351.5	6 3.594 +20 30.15	6 5.7	15 +20	30.05	1.66 -55.38	2.19	-23.40	10.5	12.0	108.2	25.7	91
1985 10 14	•0	2446352.5	6 2.504 +20 33.30	6 4-63	3C +2C	33 - 26	1.63 -55-25	2.17	-23.46	10.5	11.9	109.5	25.7	106
1985 10 15	-0	2446353.5	6 1.330 +20 36.56			36-58	1.59 -55.10		-23.51				25.6	
1985 10 16	-0	2446354.5	6 -068 +20 39-93			40.01	1.56 -54.93		-23.56				25.5	
1985 10 17	•0	2446355.5	5 58-713 +20 43-41			43.56	1.53 -54.75		-23.61				25.4	
1985 10 18	•0	2446356.5	5 57-259 +20 47-01	5 59-39			1.50 -54.54		-23-66				25.3	
1985 10 19 1985 10 20	-0.	2446357.5	5 55.701 +20 50.72			51.03	1.47 -54.32		-23.71				25.2	
	-0	2446358.5	5 54.032 +20 54.55			54.94	1.44 -54.07		-23.77				25.0	
1985 10 21 1985 10 22	•0 •0	2446359.5 2446360.5	5 52.247 +20 58.48 5 50.338 +21 2.53			58.97 3.11	1.40 -53.80		-23.82				24.8	
1985 10 23	.0	2446361.5		5 52.47			1.37 -53.50		-23.87			120.3	24.6	14 11
1985 10 23	.0	2446362.5	5 48.297 +21 6.67 5 46.117 +21 10.92	5 50-43 5 48-26		7-36 11-72	1.34 -53.17 1.31 -52.82		-23.92 -23.98			121.7	24.4	_ = = =
1985 10 25	.0	2446363.5	5 43.789 +21 15.25	5 45.93			1.28 -52.44		-24.03			124.8	24.1	109 96
1985 10 26	-0	2446364.5	5 41.304 +21 19.66	5 43.40			1.25 -52.03		-24.09			126.4	23.5	83
1985 10 27	.õ	2446365.5	5 38.651 +21 24.14	5 40.79			1.22 -51.58		-24.14			128.0	23.1	71
1985 10 28	.0	2446366.5	5 35.820 +21 28.66			29.99	1.19 -51.09		-24.19			129.6	22.7	58
1985 10 29	-0	2446367.5	5 32.800 +21 33.20	5 34.9			1.16 -50.57		-24.25			131.3	22.3	46
1985 1G 30	-0	2446368.5	5 29.579 +21 37.75	5 31.73			1.13 -50.00		-24,30			133.1	21.8	33
1985 10 31	.0	2446369.5	5 26.144 +21 42.26	5 28-29			1.11 -49.39		-24.36			134.9	21.3	21
1985 11 1	-0	2446370.5	5 22.481 +21 46.70	5 24.63			1.08 -48.73		-24.41			136.7	20.7	9
1985 11 2	- 0	2446371.5	5 18.576 +21 51.02			53.25	1.05 -48.02		-24.47			138.6	20.1	6
1985 11 3	-0	2446372.5	5 14.413 +21 55.18	5 16.34	58 +21	57.61	1.02 -47.24	1.90	-24.52	8.7	10.3	140.6	19.4	18
1985 11 4	-0	2446373.5	5 9.976 +21 59.10	5 12.13	53 +22	1.76	.99 -46.41	1.88	-24.58	8.6	10.2	142.6	18.7	31

YR	MN	DY	HR	J.D.	R.A. 1	950.0	DEC.		R.A.	APPN	E/EC.	DELTA	DELDOT	R	RDOT	M,	м ₂	THETA	BETA	300N
1985	11	5	•0	2446374.5	5 5.250	+22	2.71	5	7.407	+22	5.61	.97	-45.51	1.87	-24.64	8.5	10-1	144.7	17.9	44
1985	11	6	-0	2446375.5	5 -218	+22	5.92	5	2-374	+22	9.08		-44.53	1-85	-24.69	8.4	10.0	146.8	17.0	58
1985		7	-0	2446376.5	4 54-860	+22	8.64	4	57.016	+22	12.07		-43.48		-24.75			149.1	16.1	
1985		8	-0	2446377.5	4 49-16				51.376				-42.35		-24.80	8.2		151.4	15.1	
1985		. 9	•0	2446378.5	4 43-10			2	45.257				-41.12		-24.86	8.1		153.8	14.0	
1985			-0	2446379-5	4 36 677				38.832			-	-39.80		-24.92 -24.97	8.0 7.9		156.3 158.8	72.8 11.6	
1985 1985			•0	2446380.5	4 29.849				31.996				-38.37 -36.84		-25.03	7.8		161.5	10.2	
1985			-0	2446382.5	4 14.981				17.115				-35.20		-25.09	7.6		164.2		169
1985			.0	2446383.5	4 6.91			- 4	9.048		7.39		-33.44		-25-15	7.5		167-1		173
1985			.0	2446384.5	3 58.426			- 4		+22	.81		-31.55		-25.20	7.4		170.0		156
1985			.0	2446385.5	3 49.510			3	51.627	+21	52.05	.72	-29.54	1.71	-25.26	7.3	9.1	172.9	4.1	139
1985	11	17	-0	2446386.5	3 40.177	7 +21	33.94	3	42-284	+21	40.89	.71	-27.41		-25.32	7.2		175.8		123
1985			.0	2446387.5	3 30-44				32.537				-25-16	-	-25.37	7.1		177.7		107
1985			-0	2446388.5	3 20-32		2 • 56		22-408				-22.78		-25.43	7-1		176.1	2.3	
1985		_	-0	2446389.5			42.35		11.927				-20-29		-25.49	7.0		173.0	4.2	
1985			•0	2446390.5	2 59-07			3			27.51		-17.59		-25.54	6.9		169.6	6.3	
1985 1985			•0	2446391.5	2 48 237 2 36 776				50-073 38-801				-15.00 -12.23		-25.60 -25.65	6.8 6.7		166.0 162.3	8.5 10.8	
1985			•0	2446393.5	2 25 - 369				27.377			-63	-9.41		-25.71	6.6		158.6	13.1	18
1985			.0	2446394.5	2 13.87				15.868			-63	-6.55		-25.77	6.6		154.8	15.5	5
1985			•0	2446395.5	2 2.366			Ž			43.00	.62	-3.67		-25.92	6.5		151.0	17.9	-
1985			-0	2446396-5	1 50 90			_	52.862			-62	80		-25.37	6.4		147.2	20.2	
1985		_	.0	2446397.5	1 39.559			1	41.500	+16	17.01	-62	2.03		-25.93	6.4	8.3	143.4	22.6	40
1985	11	29	.0	2446398.5	1 28-390	+15	19.78	1	30-315	+15	30.97	-62	4.81	1.52	-25.98	6.3		139.6	25.0	
1985		36	- 0	2446399.5	1 17.45			2	19.365			•63	7.50		-26.03	6.3		135.8	27.3	
1985		7	•0	2446400.5			43.44	1			54.99	-63	10.10		-26.09	6.3		132-1	29.5	
1985		-2	-0	2446401.5	0 56-468				58.354			-64	12.58		-26.14	6.2		128.5	31.7	
1985		3	•0	2446402.5	0 46.497				48-366			-65	14.93		-26.19	6.2		124.9	33.7	
1985		4	•0	2446403.5	0 36.894				38.759			-66	17.15 19.22		-26.24	6.2		121.4	35.7 37.6	
1985 1985		5 6	.0 .0	2446404.5	0 27-697			-	20.743			-67 -68	21.14		-26.33	6.1		114.7	39.4	
1985		7	.0	2446406.5	0 10.50			_	12.346		6.35	-69	22.91		-26.38	6.1		111.5	41.1	
1985		8	.0	2446407.5	0 2.519			ŏ		_	21.61	-70	24.53		-26.42	6.1		108.3	42.7	
1985		9	-0	2446408-5					56.763			-72	26-01		-26.47	6.1		105.3	44.1	
1985		10	.0	2446409.5					49.560			•73	27.35		-26.51	6.0	1.3	102-4	45.5	131
1985	12	11	.0	2446410.5	23 40.907	7 + 6	4.93	23	42.731	+ 6	15.88	.75	28.56	1.33	-26.55	6.3	8-1	99.6	46.7	114
1985	12	12	.0	2446411.5				23	36-263	+ 5	38.69	-77	29-63		~56.59	6.0	8.1	96.8	47.9	
1935			-0	2446412.5					30-139	_	,	-79	30-59		-26.62	6.0	8.1	94.2	48.9	
1985			-0	2446413.5					24.340			-80	31.43		-26.65	6.0	8.1	91.6	49.8	
1985			.0	2446414.5					18-851			-82			-26.69	5.9	8.1	89-1	5C.7	
1985			.0	2446415.5					13.652			-84	32.80		-26.71	5.9	8.1	86-7	51.4 52.1	
1985 1985			•0	2446416.5			41.19	23 23			52.83	•86 •88	33.34 33.80		-26.74 -26.76	5.9	8.1	84.4	52.7	
1985			.0	2446418.5					59.628	_		-90	34.17		-26.78	5.9	8.1	79.9	53-1	
1985			.0	2446419.5					55.423			-92	34.47		-26.79	5.8	8.1	77.6	53.6	
1985			.0	2446420.5					51.428		7.07	.94	34.70		-26.8C	5.8	8.1	75.7	53.9	_
1985		,	•0	2446421.5					47.627			.96	34.87		-26.81	5.8	8.1	73.7	54.2	
1985	12	23	.0	2446422.5	22 42-18	5 + C	1G-38	22	44-009	+ 0	21.63	+98	34.97	1.15	-26.81	5.7	8-1	71.7	54.4	60
1985	12	24	•0	2446423.5	22 38.73	- 0	10-67	22	40.559	+ 0	.51	1.00	35.02	1.13	-26.80	5.7	8.0	69.7	54.5	73
1985			-0	2446424.5					37.266			1.02	35.02		-26.79	5.7	8.0	67-8	54.6	
1985			• 0	2446425.5					34.115			1.04	34.96		-26.77	5.6	8.0	66-0	54.6	
1985			-0	2446426.5					31.107			1.06	34.85		-26.75	5-6	8.0	64.2	54.5	
1985			-0	2446427.5					28-550			1.08	34.78	_	-26.72	5.6	8.0	62.4	54.4	
1985			•0	2446428.5					25.445			1.10	34.51		-26.68	5.5	7.9	50-6	54.2	
1985 1985			•0	2446429.5					22.786			1.12	34.27 34.00		-26.63	5.5	7.9 7.9	58.9	54.0 53.7	
1703	: 2	۱ د	•0	E44643043	FE 10-30	- 2	5 7 4 1 1	~ ~	20.222	- 2	3.31	1 - 14	J*•UU	1-03	-26.58	3.4	4.7	21.4	23.1	*00

Table B-3 (contd)

														•							
YR	М	N DY	HR	J.D.		R.A. 1	950.0	DEC.		R.A.	APPN	DEC.	DELTA	DELDOT	R	RDOT	H,	H ₂	THETA	BETA :	700N
1986		1 1	.0	2446431.5	22	15.913	3 - 2	29.01	22	17.74	; - 2	18.33	1.16	33.68	1.01	-26.51	5.4	7.9	55.5	53.4	167
1986		2	•0	2446432.5			-	-, -,		15.360		32.75	1.18	33.33		-26.43	5.3	7.8	53.9	53.0	
1986			-0	2446433.5						13.04			1.20	32.93		-26.34	5.3	7.8	52.3	52.6	
1986			-0	2446434.5				10.69		10.80		-18	1.22	32.51	-96	-26.24	5.2	7.8	50.7		137
1986			.0	2446435.5				23.72	22			13.26	1.23	32.04		-26.12	5.2	7.7	49.1	51.5	
1986	1	1 6	-0	2446436.5	22	4.675	- 3	36.37	22	6.51	- 3	25.97	1.25	31.54	-93	-25.99	5.1	7.7	47.5	5C-9	109
1986	1	7	-0	2446437.5	22	2.612	- 3	48-69	22	4.45	7 - 3	38.34	1-27	31.00	•92	-25-85	5.0	7.7	46.0	50.3	94
1986	. 1	8	-0	2446438.5	22	-598	- 4	-70	22	2.44	5 - 3	50.41	1.29	30.43	-90	-25-68	5.0	7.6	44.4	49.6	79
1986	1	1 9	-0	2446439.5	21	58-628	- 4	12.46	22	.47	1 - 4	2.22	1.31	29.82	-89	-25.50	4.9	7.6	42.9	48.8	64
1986	*	1 10	-0	2446440.5	21	56.697	- 4	23.97	21	58-541	- 4	13.79	1.32	29.18	-87	-25.29	4.8	7.5	41.4	48.0	49
1986	1	1 11	•0	2446441.5	21	54.802	2 - 4	35.28	21	56.65	- 4	25.15	1.34	28.49	-86	-25.07	4.8	7.5	39.9	47.2	35
1986	1	1 12	-0	2446442.5	21	52.937	- 4	46.42		54.79			1.36	27.78	-85	-24.82	4.7	7.4	38.4	46.2	25
1986		1 13	-0	2446443.5				57-41		52-95			1.37	27.02	-83	-24.54	4.6	7.4	36.9	45.3	13
1986		1 14	-0	2446444.5	21	49.284	- 5	8.29	21	51-147	- 4	58-32	1.39	26.23	₽82	-24.24	4.6	7.3	35.4	44.2	15
1986	1	1 15	•0	2446445.5						49.341		9.15	1.40	25.40	- 80	-23-91	4.5	7.3	34-0	43.2	25
1986		1 16	-0	2446446.5					-	47.57			1.42	24.53	• 39	-23.55	4.4	7.2	32.5	42-0	37
1986		1 17	-0	2446447.5						45.80			1.43	23.62		-23.15	4.3	7.2	31.0	4C-8	49
1986		18	-0	2446448.5			_		21	44.05	- 5	41.38	1.44	22.66	., .	-22.71	4.3	7.1	29.5	39.6	61
1986		1 19	•0	2446449.5				1.82		42-30			1-46	21.67		-22-24	4.2	7.1	28-2	38-2	73
1986		1 20	-0	2446450.5						40.563		2.87	1.47	20.64		-21-73	4.1	7.0	26.7	36.9	85
1986		1 21	•0	2446451.5						38-82			1.48	19.56		-21-17	4.0	7-0	25-3	35.4	98
1986		1 55	-0	2446452.5			-			37-084			1.49	18.44		-20-57	3.9	6.9	23.9		110
1986		23	٠0	2446453.5	-					35.343			1.50	17-27		-19.92	3.9	6.8	22.5	32-4	
1986		1 24	-0	2446454.5						33.59			1.51	16-05		-19-22	3.8	6.8	21.0		
1986		1 25	-0	2446455.5				7.28		31.84			1.52	14.79		-18.47	3.7	6.7	19.6	29-2	
1986		1 26	-0	2446456.5						30-09		9.29	1.53	13.48		-17.66	3.6	6.7	18.2	27-5	
1986		1 27	-0	2446457.5						28-32			1.54	12.12		-16.8C	3.6	6-6	16.9	25.7	
1986		1 28	-0	2446458.5						26.55			1.54	10.72		-15.88	3.5	6-6	15.5	23.9	
1986			-0	2446459.5						24,776			1.55	9.27		-14.91	3.4	6.5	14.2		154
1986		30	-0	2446460.5				5.78		22.98			1.55	7.77		-13.87	3.3	6.5	12.9	20-3	
1986			•0	2446461.5		-			-	21.18		9.09	1.56	6.23		-12.78	3.3	6.4	11.6	18.5	
1986		2 1	-0	2446462.5						19.37			1.56	4.65	-62	-11.64	3-2	6.4	10.4		
1986	-		-0	2446463.5						17-56			1.56	3.02	-61	-10.44	3.5	6.3	9-3	15.1	99
1986			-0	2446464.5						15.741			1.56	1.36	-51	-9.19	3-1	6-3	8.3	13.6	85
1986			-0	2446463.5				9.81		13.91		1.04	1.56	32	-60	-1.90	3-1	6.3	7.4	12.3	70
1986 1986			•0	2446466.5				37.21		12.074		28.57	1.56	-2.04	-60	-6.57 -5.20	3-0	6.2	6.8	11.4	56 41
	3		-0							10.23			1.56	-3.77	- 59		3-0	6-2	6.5		
1986 1986	7		•0 •0	2446468.5				51.31 5.67	21 21			42.73	1.56	-5.52 -7.28	-59	-3.80 -2.38	3.0	6.2	6.6	11.0	28 15
1986				2446470.5				20.30	_			11.86	1.56		-59	95	2-9	5.0	6.9	12.8	11
1986	•	- :	•0 •0	2446471.5				35.20	21			26.83	1.55	-9.04 -10.79	-59 -59	-49	2.9	6-1	7.6 8.5	12.2	So
1986		2 11	•0	2446472.5		_			21			42.06		-12.52	-59	1.92	3.0	6-1	9.5	16.1	32
1986		12	•0	2446473.5				5.79		59.20				-14.24	-59	3.34	3.0	6.1	10-7	18-1	45
1986		13	•0	2446474.5						57.37	-			-15.93	-59	4.75	3.0	6-1	11.9	20.1	58
1986		2 14	.0	2446475.5					20					-17.59	.59	6.13	3.0	6.1	13.2	22.3	70
1986		2 15	•0	2446476.5					-	53.75				-19.20	-60	7.47	3.1	6.2	14.5	24.4	83
1986		16	-0	2446477.5						51.96				-20.78	-60	8.78	3.2	6.2	15.9	26.6	95
1986	_	17	-0	2446478.5						50-184				-22.31	-61	10.04	3.2	6.2	17.3		107
1986		18	-0	2446479.5						48.41				-23.78	-62	11.26	3.3	6.2	18.7		119
1986		19	•0	2446480.5				1.18		46.65				-25-21	-62	12.42	3.5	6.2	20.1	33.0	
1986		2 20	-0	2446481.5						44.90				-26.58	-63	13.53	3.6	6.3	21.5		144
1986		21	-0	2446482.5						43.17				-27.89	-64	14.58	3.7	6.3	22.9	37.1	
1986		2 22	•0	2446483.5						41.44				-29.14	-65	15.58	3.9	6.3	24.3	- : "	167
1986		23	-0	2446484.5						39.72				-30-34	-66	16.51	4.0	6.4	25.8	41.0	
1986		2 24	•0	2446485.5						38.010				-31.48	-67	17.39	4.1	6.4	27.2	-	159
1986		2 25	•0	2446486.5						36-30				-3Z.57	-68	18.22	4.3	6.4	28.7	44.6	
1986		26	•0	2446487.5				-		34.593				-33.60	-69	18.99	6.4	6.5	30-1	46.4	
	•		-																		

YR	MN DY	HR	J.D.	R.A. 1950	O DEC.		R.A.	APPN	DEC.	DELTA	DELDOT	R	RDOT	м,	×2	TRETA	BETA ?	400M
1986	2 27	•0	2446488.5	20 30 884 -1	5 31.00	20 3	32.884	-15	23.79	1.31	-34.58	-70	19.70	4.5	6.5	31.6	48.0	118
1986	2 28	-0		20 29-165 -1		20 3	1.170	-15	44.34	1.29	-35.51	.71	20.37	4.6	6.6	33.0	49.6	
1986	3 1	-0		20 27.437 -1			29.448				-36.38	.72	20.99	4.7	6.6	34.5	51-1	89
1986	3 2	-0		20 25-696 -1			27.713				-37-21	-73	21.56	4.8	6.6	36.0	52.5	74
1986	3 3	-0		20 23.938 -1			25.961				~37.98	-75	22-08	4.9	6-7	37.4	53.9	60
1986	3 4	•0		20 22 157 -1			24.157				-38.71 -39 ₂ 39	.76 .77	22.5.7	5.0 5.0	6.7	38.9 40.4	55.2 56.4	45 31
1986 1986	3 5	•0		20 20 348 -1			20.548				-40.03	.79	23.42	5.0	6.8	41.9	57.6	17
1986	3 6	.0		20 16-620 -1			8.67C				-40.62	80	23.79	5.0	6.8	43.5	58.7	6
1986	3 8	.0		20 14-686 -1			6.744				-41.17	-81	24.14	5.0	6.8	45.0	59.7	13
1986	3 9	.0		20 12-695 -1			14.761				-41-67	.83	24.45	5.0	6.9	56.6	66.7	26
1986	3 10	.0		20 10-638 -1			12.712				-42-13	-84	24.73	5.0	6.9	48.1	61.5	48
1986	3 11	•0	2446500.5	20 8.505 -2	0 19.62	20 1	0.587	-20	13.34	1.04	-42-54	-86	24.99	5.0	6.9	49.7	62.4	53
1986	3 12	.0	2446501.5	20 6-285 -2	0 49.57	20	8.37€	-20	43.38		-42.90	-87	25.22	5.0	6.9	51.3	63.1	67
1986	3 13	.0	2446502.5			20	6.065				-43-22	.88	25.43	4.9	6.9	53.0	63.8	80
1986	3 14	.0	2446503.5			20	3.642				-43.49	-90	25.62	4.9	7.0	54.6	64.4	92
1986	3 15	-0		19 58.971 -2		20	1.091		- /		-43.71	-91	25.79	4.9	7-0	56.3	64.9	
1986	3 16	•0		19 56.264 -2			8.395				-43.88	-93	25.95	4.8	7-0	58.1 59.8	65.3 65.7	
1986	3 17	-0		19 53.392 -2 19 50.333 -2			55.535 52.485				-44.00 -44.05	.94	26.08	4.8	7.0	61.7	65.9	
1986 1986	3 18 3 19	-0		19 47.062 -2			9.232				-44.05	.97	26.31	4.7	7.0	63.5	66.1	
1986	3 20	-0		19 43.551 -2			5.735				-43.97	.99	26.40	4.6	7.0	65.4	66.2	
1986	3 21	-0		19 39 767 -2			1.967				-43.83	1.00	26.49	4.6	7.0	67.4	66.2	
1986	3 22	-0		19 35.672 -2	and the second s		37.89C				-43.60	1.02	26.56	4-5	7.0	69.5	66-1	
1986	3 23	-0		19 31-224 -2			3.46C		9.87		-43-28	1.04	26.62	4.5	7.0	71.6	65.9	149
1986	3 24	.0		19 26-373 -2			356.85		5.28	-71	-42.87	1.05	26.67	4.5	7.0	73.8	65.6	134
1986	3 25	-0	2446514.5	19 21.059 -3	0 8.11	19 2	23.336	-30	3.98	.69	-42.35	1-07	26.71	4.4	7.0	76.1	65.2	119
1986	3 26	.0	2446515.5	19 15.216 -3			17.516		6.15		-41.71	1.08	26.74	4.4	6.9	78.5	64-6	
1986	3 27	-C	2446516.5				1.09C			-	-40.94	1.10	26.77	4.3	6.9	81.0	63.9	8.8
1986	3 28	-0	2446517.5			19	3.965				-40-01	1.11	26-79	4-3	6.9		63.0	71
1986	3 29	-0		18 53-650 -3			6.034				-38.91	1.13	26.80	4.2	6.9	86.4	62.0	55
1986	3 30	-0		18 44-758 -3			7.174				-37-61	1.14	26.81	4.2	6.9	89.2	8-06	39
1986	3 31	-0		18 34.790 -3			37.241				-36.09	1.16	26.81	4.1	6.8	92.3 95.5	59.4 57.9	24 11
1986 1986	4 1	.0		18 23.586 -3 18 10.970 -3			26.074 13.495				-34-33 -32-30	1.19	26.80 26.79	4.1	6.8	98.9	56.1	15
1986	4 3	-0		17 56-752 -4			59.315	_			-29-98	1.21	26.78	4.0		102-4	54.1	29
1986	4 4	.0		17 40.750 -4			3.347				-27.33	1.22	26.77	4.0		106.2	51.9	45
1986	4 5	.0		17 22.802 -4			25.43C				-24.35	1.24	26.75	4.0		110.1	49.5	61
1986	4 6	.0	2446526.5				5.455				-21.02	1-25	26.72	4.0	5.7	114.1	46.8	77
1986	4 7	-0	2446527.5	16 40.781 -4	6 15.72		3.436				-17-35	1-27	26.69	4.0	5.7	118.3	44.1	92
1986	4 8	.0	2446528.5	16 16.875 -4	7 .34	16 1	19.520	-47	5.57	.43	-13.37	1-28	26.66	4.0		122-6	41.1	
1986	4 9	-0		15 51.450 *4			54.062			.42	-9.11	1.30	26-63	4.0		726.8	38.1	
1986	4 10	-0		15 25.059 -4			27.616			.42	-4.64	1.31	26.60	4.0		131.0	35.1	3 19 1
1986	4 11	-0		14 58-399 -4		15			17.23	-42	03	1-33	26.56	4.0		135.0	35-5	
1986	4 12	-0		14 32-212 -4			34-607			-42	4.62	1.34	25.52	4.1		138.8	29.4	
1986	4 13	-0		14 7.168 -4		14	9.471	-		-42	9.23	1.36	26.48	4.1		142.1	26.9	
1986	4 14	-0		13 43.775 -4 13 22.340 -4			45.98E			-43	13.70 17.97	1.37	26.44	4.2		144.9	24.2	
1986 1986	4 15	-0		13 22.340 -4			5.041			.44	21.98	1.41	26.35	4.4		148.5	21.9	
1986	4 17	•0		12 45.678 -3			7.677			-46	25.69	1.42	26-30	4.5		149.3	21.2	98
1986	4 18	.0		12 30.311 -3			392-28			-48	29.08	1.44	26.25	4-6		149.3	20.9	83
1986	4 19	-0		12 16.711 -3	-		18.621			-50	32-16	1.45	26.20	4.7		148.8	21.0	69
1986	4 20	-0		12 4-691 -3			6.570			-51	34.93	1.47	26-15	4.8		147.8	21.4	56
1986	4 21	.0		11 54-068 -3			55.92			-54	37.41	1.48	26-10	4.9	7.9	146.4	22.1	43
1986	4 22	-0	2446542.5	11 44.665 -2	9 30-18		6-501			-56	39.62	1.50	26.05	5.1		144.8	22.8	33
1986	4 23	-0		11 36-329 -2			38.15C			-58	41-59	1.51	29-00	5.2	-	143.1	23.6	29
1986	4 24	-0	2446544.5	11 28-919 -2	6 24.37	11 3	30.73C	-26	36,51	.61	43.34	1.53	25.95	5.3	8.2	141.3	24.4	34

YR	MN DY	HR	J.D.		R.A.	1950.0	DEC.		R.A.	APPN	BEC.	DELTA	DELDOT	R	RDOT	×,	Ħ,	THETA	BETA	MOON
1986	4 25	-0	2446545.5	11	22.31	8 -25	- 10	11	24.120	-55	12.18	-63	44.89	1.54	25.89	5.4	8.4	139.4	25.1	44
1986	4 26	-0	2446546.5						18.217			-66	46.28	1.56	25.84	5.5		137.5	25.9	57
1986	4 27	+0	2446547-5	. ,-				11				-68	47-50	1-57	25.78	5.6		135.7	26.6	72
1786	4 28	-0	2446548-5				19.74	11			31.66	-71	48.60	1.59	25.73	5-8		133.8	27.3	86
1986	4 29	-0	2446549.5				16.15	11			28.01	.74	49.58	1-60	25.67	5.9		132.0	27-9	
1986	4 30	.0	2446550.5					11			28.77	-77	50.45	1.62	25.62	6-D		130.3		114
1986 1986	5 1	-0	2446551.5						56.607			.80 .83	51.23 51.93	1.63	25.56	6.3		128.6 126.9	28.9	127
1986	5 2 5 3	.0 .0	2446553.5						50.614			-86	52.55	1.66	25.45	6.3		125.3	29.7	
1986	5 4	-0	2446554.5						48.03			-89	53.11	1.67	25.39	6.3		123.7		
1986	5 5	-0	2446555.5						45.689			-92	53.61	1-69	25.33	6.4		122.2	30.4	
1986	5 6	.0	2446556-5						43.560			.95	54.06	1-70	25-28	6.5		120.7	30.6	
1986	5 7	.0	2446557.5						41.624			-98	54.47	1.72	25.22	6.6		119.2		
1986	5 8	.0	2446558.5						39.865			1.01	54.83	1.73	25.16	6.7		117.8	31.0	127
1986	5 9	.0	2446559.5	10	36.47	2 -12	55.30		38.26			1-05	55.15	1.75	25.11			116.4	31.2	116
1986	5 10	-0	2446560.5	10	35-01	7 -12	25.44	10	36.81	-12	36.82	1.08	55.43	1.76	25.05	6.8	10.1	115.0	31.3	105
1986	5 11	-0	2446561.5	10	33.69	5 -11	57.42	10	35.490	-12	8.75	1.11	55.69	1.78	24.99	6.9	10.2	113.7	31.4	94
1986	5 12	-0	2446562.5						34-291			1.14	55-91	1.79	24.94			112.4	31.4	82
1986	5 13	-0	2446563.5						33-204			1-17	56-11	1.81	24.88			111.2	31.5	71
1986	5. 14.	.0	2446564-5						32.219			1.21	56-28	1-82	24-82			109.9	31.5	60
1986	5 15	-0	2446565-5						31.330			1.24	56.43	1-83	24.77			108.7	3%5	49
1986	5 16	.0	2446566-5						30-529			1.27	56.56	1-85	24.71			107-5	31.5	38
1986	5 17	.0	2446567-5						29-808			1.31	56.67	1-86	24.65			106.3	31.4	28
1986	5 18	-0	2446568-5						29-163			1.34	56.76	1.88	24.60			105.2	31.3	22
1986	5 19	-0	2446569.5						28.588			1.37	56-83	1.89	24.54			104.0	31.3	22
1986 1986	5 20	-0	2446570.5						28-078			1-40	56,89	1.90	24.49			102.9	31.2	29 40
1986	5 21 5 22	-0 -0	2446571.5 2446572.5						27.628			1.44	56-93 56-96	1.92	24.43			100.7	37.0	53
1986	5 23	-0	2446573.5						26.89			1.50	56.98	1.95	24.32		11.3	99.6	30.8	67
1986	5 24	-0	24-6574-5						26.604		4.86	1.54	56.98	1.96	24.27		11	98.6	30.7	81
1986	5 25	.0	2446575.5						26-361			1.57	56.97	1.98	24.21		11.4	97.5	30.6	96
1986	5 26	.0	2446576.5						26-159			1.60	56.95	1.99	24.16		11.5	96.5	30.4	110
1986	5 27	.0	2446577.5						25.999			1.63	56-93	2.00	24.10		11.6	95-5	30.2	
1986	5 28	-0	2446578.5						25.87			1.67	56.89	2.02	24.05		11.7	94.5	30.1	
1986	5 29	.0	2446579.5			-			25-794			1.70	56-84	2.03	24.00		11.7		29.9	
1986	5 30	.0	2446580.5						25.74		1.56	1.73	56-78	2-04	23.94	8.0	11.8	92.5	29.7	157
1986	5 31	+0	2446581-5						25.72			1.77	56-71	2-06	23.89	3.1	11.9	91.5	29.5	160
1986	6 1	-0	2446582.5	10	23.92	3 - 6	33.81	10	25-739	- 6	44-512	1.80	56-64	2.07	23.84	8.1	11.9	90.5	29.3	155
1986	6 2	.0	2446583.5	10	23.96	5 - 6	26-20	10	25.781	1 - 6	37.31	1.83	56-55	2-09	23.78	8.2	12.0	89.6	29.1	146
1986	6 3	-0	2446584.5					10	25-857	2 - 6	30-14	1.86	56-46	2-10	23.73	8.2	12-1	88.6	28.9	136
1986	6 4	-0	2446585-5						25.948			1.90	56-36	2.11	23.68		12.1	87.7	28.7	
1986	6 5	.0	2446586-5						26.070			1.93	50.25	2.13	23.63		12.2	86.7	28.4	
1986	6 6	-0	2446587.5						26-21			1.96	56.13	2.14	23.58		12.3	85.8	25.2	
1986	6 7	-0	2446588-5					10				1.99	56.00	2.15	23.52		12.3	84.9	25.0	
1986	6 8	-0	2446589.5	_					26.573		-35	2.03	55.86	2-17	53-65		12.4	84.0	27.7	
1986	6 9	-0	2446590.5						26.783			2.06	55.72	2-18	23.42		12.5	83.0	27.5	69
1986 1986	6 10	-0	2446591.5						27.017			2.09	55.57 55.41	2-19	23.37		12.5	82-1 81-2	27.0	58 47
	6 12	-0	2446593.5						27-525				55.25	5-55	23.27		12.6	80.3	20.8	36
1986 1986	6 13	-0	2446594-5						27.80			2.15	55.08	2.24	23.22		12.7	79.5	26.5	28
1986	6 14	.0	2446595.5						28-10			2.22	54.90	2.25	23.17		12.7	78.6	26.3	19
1986	6 15	.0	2446596.5						28-419				54.71	2.26	23-12		12.8	77.7	26.0	
1986	6 16	.0	2446597.5						28.74			2-28	54.52	2:28	23.07		12.9	76.8	25-8	52
1986	6 17	.0	2446598.5						29.08			2.31	54.33	2-29	23.03		12.9	76.0	25.5	35
1986	6 18	.0	2446599-5					10				2.34	54.12	2.30	22-98		13-0	75.1	25.2	-
1986	6 19	.0	2446600.5						29.81			2.37	53-91	2-32	22.93		13.0	74.2	25.0	61
1986	6 20	-0	2446601.5			-			30-189			2.41	53.70	2.33		9.1	,	73.4	24.7	75
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YR	MN DY	HR	J.D.	R.A.	950.0	DEC.	R.	Α.	APPN	DEC.	DELTA	DELDOT	R	RDOT	H	M ₂	THETA	BETA	MOON
1986	6 21	-0	2446602.5	10 28.75	7 - 5	7.33	10 30	.580	- 5	18,52	2.44	53.48	2.34	22.83	9.1	13-1	72.5	21.5	90
1986	6 22	.0	2446603.5	10 29.15	9 - 5	5.75	10 30	982	- 5	16,94	2.47	53.26	2.35	22.79		13.2	71.7	24.2	104
1986	6 53	-0	2446604.5			4-36	10 31	.394	- 5	15,56	2-20	53.03	2.37	22.74	9.2	13.2	70.8	23.9	118
1986	6 24	-0	2446605.5			3.16				14 ,36	2.53	52-80	2-38	22.69		13.3	70.0	23.6	
1986	6 25	-0	2446606-5			2.13				13 ,35	2.56	52.56	2-39	22.65		13.3	69.2	23.4	
1986	6 26	-0	2446607.5			1.28			-	12,50	2.59	52.32	2.41	22.60		13.4	68.3	23-1	
1986 1986	6 27	-0	2446608.5			-59			-	11.82	2.62	52-08	2.42	22.55		13.4	67-5	22-8	
1986	6 28 6 29	.0 .0	2446610-5			-07				11,31	2-65	51.82 51.57	2.43	22-51		13.5	66-7 65-9	22.6	
1986	6 30	.0	2446611.5		•					10,74	2.68	51.30	2.45	22.42		13.5 13.6	65-0	22.3	
1986	7 1	.0	2446612.5				- :			10.68	2.74	51.03	2.47	22.37		13.6	64-2	21.7	
1986	7 2	-0	2446613.5							10.77	2.77	50.76	2.49	22-33		13.7	63.4	21.5	
1986	7 3	-0	2446614.5		_					11.00	2.80	50.48	2.50	22.29		13.7	62.6	21.2	
1986	7 4	.0	2446615.5		-	.07				11.36	2.83	50.20	2.51	22.24		13.8	61.8	20.9	97
1986	7 . 5	.0	2446616.5	10 35-19	8 - 5	-56				11 .85	2.86	49.91	2.52	22.20	9.8	13.8	61.0	20.6	85
1986	7 6	-0	2446617.5	10 35.71	4 - 5	1.17	10 37	-535	- 5	12.48	2.88	49.62	2.54	22-15	9.9	13.8	60.2	20.3	74
1986	7 7	-0	2446618.5			1.91				13 22	2.91	49.32	2.55		9.9		59.4	20.1	63
1986	7 8	-0	2446619.5			2.76					2.94	49.01	2.56	22.07			58.6	19.8	
1986	7 9	-0	2446620.5			3.74	10 39			> .07	2.97	48.71	2.57	55-05			57.8	19.5	
1986	7.10	•0	2446621.5			4.83				16.17	3-00	48.39	2.59	21.98			57.0	19.2	
1986	7 11	•0	2446622.5			6-02				17,37	3.03	48.07	2.60	21-94			56-2	19.C	
1985 1986	7 12	-0	2446623.5			7-33				18 469	3-05	47.75	2-61	21.90			55.4	18.7	15
1986	7 13 7 14	.0	2446624.5			8.74				20.10	3.08	47.43	2.63	21.86			54.6 53.8	18.4	19 29
1986	7 15	-0	2446626.5							23,24	3.13	45.76	2.65	21.77			53.0	17.8	41
1986	7 16	-0	2446627.5				-		_	24.96	3.16	46.42	2.66	21.73			52.2	17.6	
1986	7 17	-0	2446628.5		-					26 76	3.19	46.08	2.68	21.69			51.5	17.3	
1986	7 18	.0	2446629.5							28,66	3.21	45.74	2.69	21.65			50.7	17.0	
1986	7 19	-0	2446630.5	10 42.86	5 - 5	19.23				30.65	3.24	45.39	2.70	21.61			49.9	14.7	
1986	7 20	-0	2446631.5	10 43-44	2 - 5	21.29	10 45	-266	- 5	32 .72	3.27	45.04	2.71	21.57	10.6	14.4	49.1	16.4	169
1986	7 21	•0	2446632.5	10 44-02	1 - 5	23.43	10 45	.84€	- 5	34 #87	3.29	44.68	2.73	21.53	10.6	14.4	48.3	16.2	123
1986	7 22	-0	2446633.5	10 44.60	2 - 5	25.66	10 46	.427	- 5	37411	3.32	44.33	2.74	21.49	10.7	14.5	47.6	15.9	137
1986	7 23	-0	2446634.5							39,42	3.34	43.96	2.75	21.45			46.8	15.5	
1986	7 24	-0	2446635.5							41,81	3.37	43.60	2.76	21.41			46.0	15.3	
1986	7 25	-0	2446636.5							44 28	3.39	43.23	2.78	21.37			45.3	15.1	
1986	7 26	-0	2446637.5							46482	3.42	42.86	2.79	21.34			44.5	14.8	
1986 1986	7 27	-0	2446638.5	.,	-					49,43	3.44	42.49	2-80	21.30			43.7	14.5	
1986	7 28 7 29	.0 .0	2446640.5							52 -12 54 -87	3.47	42.11	2.81	21.26			43.0	14.2	/
1986	7 30	-0	2446641.5							57 469	3.52	41.34	2.84	21.78			41.5	13.7	
1986	7 31	.0	2446642.5				10 51		_	458	3.54	40.95	2.85	21-15			40.7	13.4	
1986	5 1	-0	2446643.5				10 52		_	3,53	3.56	40.56	2.86	21.11			39.9	13.2	
1985	8 2	.0	2446644.5				10 52			6455	3.59	40.16	2.87	21.07			39.2	12.9	
1986	8 3	-0	2446645.5						_	9 462	3.61	39.76	2.89	21.03			38.4	12-6	
1986	8 4	-0	2446646.5	10 52.35	0 - 6	1.20	10 54	.175	- 6	12.76	3.63	39.35	2.90	21.00	11.3	14.9	37.7	12.4	58
1986	8 5	-0	2446647.5	10 52-95	5 - 6	4.39	10 54	.78C	- 6	15 .96	3.66	38.95	2.91	20.96	11.4	15.0	36.9	12.1	47
1986	8 6	-0	2446648.5		-		10 55	-387	- 6	19.21	3.68	38.54	2.92	20.92	11.4	15.0	36.2	11.8	36
1986	ε 7	-0	2446649.5							22.53	3.70	38.12	2.93	20.89			35.4	11.6	
1986	8 8	-0	2446650.5							25 489	3.72	37.70	2-95	20.85			34.7	11.3	
1986	8 9	-0	2446651.5							29.31	3.74	37-28	2.96	20.82			34.0	11.0	-
1986	8 10	>0 0	2446652-5							32.78	3.77	36.86	2-97	20.78			33.2	10.8	
1986 1986	8 11 8 12	•0	2446654.5						_	36 +3C	3.79	36.43	2.98	20.74			32-5	10-5	
1986	8 13	.0	2446655.5							39.88 43.50	3.81 3.83	36.01 35.58	2.99 3.01	20.71			31.8	10-3	-
1986	8 14	.0	2446656-5				11			47,17	3.85	35.14	3-05	20.64			30.3	15.0	
1986	8 15	•0	2446657.5				11			50.88	3.87	34.71	3.03	20.61			29.6	9.5	
1986	8 16	-0	2446658.5		-					54,64		34.27	3.04	20.57			28.9		100
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YR	MN DY	HR	J.D,	R.A. 1950.0 DEC.		R.A. APPN	DEC.	DELTA	DELDOT	R	RDOT	H,	M ₂	THETA	BETA 3	MOON
1986	8 17	-0	2446659.5	11 .246 - 6 46.77	11	2.071 - 6	58.44	3.91	33.83	3.05	20.54	12.0	15.3	28.2	9.0	114
1986	8 18	•0	2446660.5		11	2.677 - 7		3.93	33.39	3.07	20.50	12.0	15.3	27.5	8.8	128
1986	8 19	.0	2446661.5		11	3.282 - 7		3.95	32.95	3.08		12.1		26.8	8.5	
1986 1986	8 20 8 21	•0	2446662.5		11	3-886 - 7		3.97	32.51	3.09		12.1		26.1	8.3	
1986	8 22	•0	2446663.5 2446664.5		11	4.485 - 7		3-98	32.07	3.10		12.2		25.4	8.0	
1986	8 23	.0	2446665.5		11	5.091 - 7 5.892 - 7		4.00	31.62 31.17	3.11 3.12		12.2		24.7	7.8	
1986	8 24	.0	2446666.5		11	6.292 - 7		4.04	30.72	3.14		12.3		24.0	7•6 7•3	
1986	8 25	•0	2446667.5		11	6.890 - 7		4.06	30.26	3.15		12.3		22.6	7.1	
1986	٤ 26	-0	2446668.5	11 5.663 - 7 22.72	11	7.488 - 7		4.07	29.81	3.16		12.4		22.0	6.9	
1986	δ 27	-0	2446669.5	11 6-259 - 7 26.90	11	8.084 - 7	38 .64	4.09	29.35	3.17		12.4		21.3	6.7	
1986	8 28	•0	2446670.5		11	8.678 - 7		4.11	28.89	3.18	20.17	12.5	15.6	20.7	6-4	100
1986	8 23	•0	2446671.5		11	9.271 - 7		4.13	28.43	3.19	20.14	12.5	15.6	20.1	6.2	89
1986	8 30.	• 1.	2446672.5		11	9.863 - 7		4.14	27-96	3.21		12.5		19.4	6.0	78
1986	8 31	-0	2446673.5			10.452 - 7		4.16	27.49	3.22		12-6		18.8	5.8	66
1986 1986	9 1 9 2	•0	2446674.5 2446675.5			11-046 - 8	.07	4.17	27.02	3.23		12.6		18.2	5.6	55
1986	9 3	.0		; 11 9.799 - 7 52.07 ; 11 10.382 - 7 57.08		11.625 - 8		4.19	26.55	3.24		12.7		37.7	5.4	43
1986	9 4	-0		17 10.963 - 8 1.51			13,30	4.20	26.08 25.61	3.25		12.7		17.1	5.2	32
1986	9 5	•0		11 11.542 - 8 5.97		13.368 - 8		4.23	25.13	3.28		32.8		16.6 16.0	5.1 4.9	22 15
1986	9 6	•0		11 12.118 - 8 10.46		13.944 - 8		4.25	24.65	3.29		12.8		15.5	4.7	17
1986	9 7	•0		11 12.692 - 8 14-97		14.518 - 8		4.26	24.17	3.30		12.9		15.1	4.6	27
1986	98	•0		11 13.263 - 8 15.51		15.085 - 8		4.27	23.69	3.31		12.9		14.6	4.4	39
1986	9 9	-0	2446682.5	11 13.831 - 8 24.08	11	15.657 - 8	35.90	4.29	23.22	3.32		12.9		14.2	4.3	52
1986	9 10	-0		11 14.396 - 8 28.66		16.223 - 8		4.30	22.74	3.33	19.77	13.0	15.9	13.8	4.1	65
1986	9 11	-0		11 14.958 - 8 33.27		16.785 - 8		4.31	22.25	3.34		13.0		13.5	4.0	79
1986.	9 12	-0		11 15.517 - 8 37.91		17.344 - 8		4-33	21.77	3.36		13.0		13.2	3.9	92
1986 1986	9 13 9 14	•0		11 16.073 - 8 42.56		17.901 - 8		4.34	21.29	3.37		13.1		13.0	3.8	
1986	9 15	.0		i 11 16.625 - 8 47.23 i 11 17.174 - 8 51.92		18.453 - 8 19.003 - 9		4.35	20.81	3.38		13.1		12.8	3.8	
1986	9 16	•0		11 17.720 - 8 56.63		19.568 - 9		4.36	20.33 19.85	3.39 3.40		13.1		12.6	3.7	
1986	9 17	.0		11 18.262 - 9 1.36			13.23	4.39	19.37	3.41		13.2		12.5	3.7 3.6	
1986	9 18	.0		11 18.800 - 9 6.11	11			4.40	18.89	3.42		13.2		12.4	3.6	
1986	9 19	.0		11 19.335 - 9 10.87	11	21.164 - 9		4.41	18.41	3.43		13.3		12.5	3.6	
1986	9 20	•0	2446693.5	11 19.866 - 9 15.65	11	21.695 - 9	27.53	4.42	17.93	3.45		13.3		12.6	3.6	
1986	9 21	-0		11 20.392 - 9 20.45	11	22.222 - 9	32.33	4.43	17.45	3.46		13.3		12.8	3.7	
1986	9 22	•0		11 20-915 - 9 25-26		22.745 - 9		4.44	16.96	3.47	19.42	13.3	16.1	13.0	3.7	131
1986	9 23	•0		11 21.434 - 9 30.08		23-264 - 9		4.45	16.48	3.48		13.4		13.2	3.8	120
1986	9 24	-0		11 21.948 - 9 34.92		23.778 - 9		4.46	16.00	3.49		13.4		13.5		109
1986 1986	9 25 9 26	•0 •0		i 11 22.459 - 9 39.78 i 11 22.964 - 9 44.64		24-285 - 9		4.47	15.51	3.50		13.4		13.9	3.9	97
1986	9 27	.0		11 23.466 - 9 49.52	11	24.795 - 9 25.296 -10		4.48	15.03	3.51		13.5		14.3	4.0	86
1986	9 28	•0		11 23.962 - 9 54.41		25.793 -10		4.48	14.55	3.52 3.54		13.5 13.5		14.7	4-1	75
1986	9 29	.0		11 24.454 - 9 59.32		26.285 -10		4.50	13.58	3.55		13.5		15.1 15.6	4.2	63 52
1986	9 30	•0		11 24.941 -10 4.23		26.773 -10		4.51	13.10	3.56		13.6		16.1	4.5	40
1986	10 1	.0		11 25.423 -10 9.15		27.255 -10		4.52	12.61	3.57		13.6		16.7	4-6	29
1986	16 2	•0	2446705.5	11 25.899 -10 14.08		27.732 -10		4.52	12.13	3.58		13.6		17.3	4.8	19
1986		-0		11 26.371 -10 19-92	11	28.203 -10	30.96	4.53	11.65	3.59		13.6		17.9	4.9	74
1986		-0		11 26.837 -10 27 ``		28.670 -10		4.54	11.17	3-60	19.08	13.6	16.3	18.5	5.0	20
1986		-0		11 27-297 -10 26		29.13€ -70		4.54	10.69	3.61		13.7		19.1	5.2	31
1986	-	•0		11 27-752 -10 33-60		29.585 -10		4.55	10.21	3.62		13.7		19.7	5.3	44
1986 1986		•0 •0		11 28.201 -10 38.84 11 28.644 -10 43.80		30-035 -10		4.55	9.73	3.63		13.7		20.4	5.5	58
1986		•0		11 29.087 -10 48.77		30.478 -10 30.916 -11	.73	4.56	9-26	3.65		13.7		21.1	5.7	71
1986		.0		11 29.511 -10 53.74		31.347 -11	5.71	4.57 4.57	8.79 8.32	3-66 3-67		13.7 13.8		21.8	5-8	85
1986		.0		11 29.936 -10 58.72		31.772 -11		4.58	7.85	3.68		13.8		23.2	6.0 6.1	99 112
	1G 12	-0		11 30-354 -11 3-69		32.196 -11		4.58	7.38	3.69		13.8		23.9	6.3	
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1986	1G 1	3	•0	2446716.5	11 30.765 -11	8.66 1	1 32.602 -1	20.64	4.58	6.92	3.70	18.85	13.8	16.5	24.7	6.5 13	8
1986	10 1	4	-0	2446717.5	11 31.170 -11	13.63 1	1 33.007 -1	25.61	4.59	6.46	3.71	18.82	13.8	16.5	25.4	6.6 15	0
	10 1		-0		11 31.568 -11		1 33.405 -1		4.59	6.00	3.72	18.80			26.2	6.8 16	
	10 1		-0		11 31.959 -11		1 33.796 -1		4.59	5-54	3.73	18.77			26.9	6.9 16	
	10 1		-0		11 32-343 -11		1 34.181 -1		4.60	5.09	3.74	18.75			27.7	7.1 15	
	10 1		•0		11 32.720 -11		1 34.558 -1		4.60	4-64	3.75	18.72			28.5	7.3 15 7.4 13	
	10 1 10 2		•0		11 33.089 -11 3 11 33.451 -11		1 34.928 -1 1 35.290 -1		4-60 4-61	4.19 3.74	3.77 3.78	18.70	13.9		29.3 30.0	7.6 12	
	16 2		•0		11 33.806 -11		1 35.645 -1		4.61	3.30	3.79	18.65			30.8	7.7 11	
	10 2	-	•0		11 34-153 -11		1 35.993 -1		4.61	2-86	3.80	18.62			31.6	7.9 10	
	16 2		.0		11 34.492 -11		1 36-333 -1		4.61	2.42	3.81	18.60			32.5		33
	10 2		•0				1 36.665 -1		4.61	1.98	3.82	18-57	14-0	16.6	33.3	8.2 8	58
1986	10 2	5	•0	2446728.5	11 35.147 -12	8.08 1	1 36.988 -1	20.09	4,61	1.54	3.83	18.55	14.0	16.7	34.1	8.4 7	71
1986	10 2	6	-0	2446729.5	11 35.462 -12		1 37.304 -1		4.61	1.11	3.84	18.52			34.9		59
1986	10 2	7	•0		11 35.769 -12		1 37.611 -1		4.61	-68	3.85	18.50			35.7		8
	10 2		• Ü		11 36.067 -12		1 37.909 -1		4-61	-26	3.86	18.48			36.6		37
	10 2		•0	-	11 36.356 -12		1 38.199 -1		4.61	17	3.87	18.45			37-4		26
	10 3		-0		11 36-636 -12		1 38.480 -1		4.61	59	3.88	18.43			38-3		17
	10 3		-0		11 36.908 -12		1 38.752 -1		4.61	-1.00	3.89	18.40 18.38			39.1 40.0		16 24
1986 1986		1 2	•0		11 37.170 -12 (1 39.014 -1 1 39.268 -1		4.61	-1.41 -1.82	3.90 3.92		14.0		40.8	-	56
1986		3	-0		11 37.666 -12		1 39.511 -1		4.61	-2.25	3.93	18.33			41.7		5 C
1986		4	•0		11 37.900 -12		1 39.746 -1		4.61	-2.62	3.94		14.0		42.6		54
1986		5	•0		11 38.124 -13		1 39.970 -1		4.61	-3.01	3.95		14.1		43.4		78
1986		6	-0		11 38.337 -13		1 40-184 -1		4.61	-3.40	3.96		14.1		44.3) Ž
1986		7	•0		11 38-541 -13	10.83 1	1 40.388 -1	22.87	4.60	-3.78	3.97	18.24	14.1	16.8	45.2	10.2 10	16
1986	11	8	-0	2446742.5	11 38.734 -13	15.52 1	1 40.582 -1	3 27.57	4-60	-4-15	3.98	18.22	14.1	16.8	45.1	10.3 11	19
1986		9	• 0		11 38.917 -13		1 40.765 -1		4.60	-4.52	3.99		14.1		46.9	10.5 13	
1986			•0		11 39.088 -13		1 40.937 -1		4.60	-4.89	4.00		14.1		47.8	9C.6 14	
	11 1		٠0		11 39.250 -13		1 41.095 -1		4.59	-5.25	4.01		14.1		48.7	10.7 15	
	11 1		•0		11 39 400 -13		1 41.245 -1		4.59	~5.60	4.02		14.1		49.6	10.8 16	
	11 1		•0		11 39.539 -13		1 41.389 -1		4.59	-5.95	4.03		14.1		50.5	10.9 16	
	11 1		•0		11 39.667 -13 4 11 39.783 -13		1 41.517 -1 1 41.634 -1		4.58 4.58	-6.29 -6.62	4.04 4.05	18.06	14.1		51.4 52.3	11.0 15	
	11 1		•0		11 39.888 -13		1 41.735 -1		4.58	-6.95	4.06		14.1		53.3	11.2 13	
	11 1		.0		11 39.981 -13		1 41.833 -1	- ,	4.57	-7.28	4.07		14.1		54.2	11.4 12	
	11 1		•0		11 40.062 -14		1 41.914 -1		4.57	-7.60	4.08		14.1		55.1	11-5 11	
	11 1		.0		11 40.131 -14		1 41.984 -1		4.56	-7.91	4.09	17.97	14.1	16.9	56.0	11.5 9	9
1986	11 2	0	•0	2446754.5	11 40.188 -14	9.74 1	1 42.041 -1	21.81	4.56	-8.22	4.10	17.95	14.1	16.9	57.0	11.6 8	38
1986	11 2	1	٠0		11 40.233 -14		1 42.086 -1	26.12	4.55	-8.52	4.11	17.93			57.9		76
	11 2		•0		11 40.265 -14		1 42.115 -1		4.55	-8.81	4.12		14.1		58.8		55
	11 2		-0		11 40.284 -14		1 42.139 -1		4.54	-9.10	4.14	17.88			59.8		54
	11 2		-0		11 40-290 -14		1 42.145 -1		4.54	-9.38	4.15		14.1		60.7		43
	11 2		•0		11 40.283 -14		1 42.135 -1		4.53	-9.65	4.16	17.84			61.7		32
	11 2		•0		11 40.263 -14 1 11 40.230 -14 1		1 42.115 -1 1 42.086 -1		4 - 53.	-9.92 -10.17	4.17 4.18	17.80	14-1		62.6 63.6		22 17
	11 2		•0		11 40.183 -14		1 42.039 -1			-10.42	4.19	17.78			64.5		20
	11 2		•0		11 40 122 -14		1 41.975 -1			-10.67	4.20	17.76			65.5		30
1986			•0		11 40.047 -14		1 41.904 -1			-10.90	4.21		14.1		66-4		42
1986		1	.0		11 39.958 -14		1 41.815 -1			-11.13	4.22	17.71			67.4		56
1986		2	•0		11 39-854 -14		1 41.712 -1			-11.34	4.23	17.69			68.4		70
1986		3	.0		11 39.736 -15		1 41.595 -1	5 14.42		-11.55	4.24	17.67	14.1	17.0	69.4	12.6 8	35
1986		4	•0		11 39.604 -15		1 41.463 -1			-11.75	4.25		14.1		70.4		99
1986		5	-0		11 39.456 -15		1 41.316 -1			-11.94	4.26		14.1		71.3	12.7 11	
1986		6	-0	-	11 39.294 -15		1 41.154 -1			-12.12	4.27		14-1		72-3	12.7 12	
1986		7	•0		11 39-116 -15		1 40.976 -1			-12.28	≟-28	17.59			73.3	12.7 14	
1986	12	8	•0	2440/12.5	11 38.923 -15	20-16 1	1 40.784 -1	> 32.28	4.45	-12.44	4.29	17.57	14.1	17.1	74.3	12.8 15	, 1

YR	MN DY	HR	J.D.	R.A. 1950.0	DEC.	R.A. APPN	DEC.	DELTA D	ELDOT	R	RDOT	M	M ₂	THETA	LETA	MOON
	12 9	-0	2446773.5	11 38.715 -15	23.54 11	40.576 -15	35.66	4.44 -	12.59	4.30	17-55	14-1	17.1	75.3	12-8	160
	12 10	•0	2446774.5	11 38.491 -15	26.85 11	40.352 -15	38.97	4.43 -		4.31	17.53			76.3	12-8	
	12 11	•0		11 38.252 -15		40.113 -15		4.43 -		4.32	17.51			77.3	12.9	156
	12 12	•0		11 37.997 -15		39.858 -15		4-42 -		4.33	17.49			78.3	12.9	
	12 13	•0		11 37.726 -15		39.588 -15		4.41 -		4.34	17.47			79.4	12.9	
	12 14	•0		11 37.439 -15 11 37.137 -15		39.301 -15 38.999 -15		4.40 -		4.35	17.45			80-4	12.9	
	12 16	.0		11 36.818 -15		38.68C -15		4.40 -		4.36 4.37	17.43 17.41			81.4	12.9	102
	12 17	•0		11 36.482 -15		38.345 -16	.14	4.38 -		4.38	17.39			82.4 83.5	12.9	91
	12 18	•0		11 36.131 -15		37.993 -16	2.85	4.37 -		4.39	17-37			84.5	12.9	79
1986	12 19	•0		11 35.762 -15		37.626 -16	5.48	4.37 -		4.40	17.35			85.5	12.9	68
1986	12 20	-0		11 35.378 -15		37-241 -16		4.36 -		4.41	17.33			86.6	12.9	57
1986	12 21	-0	2446785.5	11 34.976 -15		36-84C -16		4.35 -		4.42	17.31			87.6	12.8	46
	12 22	•0		11 34.558 -16		36.421 -16	12.84	4.34 -	13.63	4.43	17.29	14.1	17.2	88.7	12.8	35
	12 23	•0		11 34.123 -16		35.986 -16	15.11	4.33 -	13.64	4.44	17.27	14.1	17.2	89.7	12.8	26
	12 24	•0		11 33.671 -16		35-534 -16		4.33 -		4.45	17.25			90.8	12.8	19
	12 25	•0		11 33.202 -16				4.32 -		4.46	17.23			91.8	12.7	20
	12 28	•0		11 32.716 -16				4.37 -		4.47	17.21			92.9	12.7	27
	12 27 12 28	•0 •0		11 32.213 -16 11 31.692 -16		34-076 -16		4-30 -		4.48	17.20			94.0	12.7	38
	12 29	-0		11 31.155 -16		33.556 -16 33.018 -16		4.29 -		4.49 4.50	17.18 17.16			95.0	12.6	51 65
	12 30	-0		11 30.600 -16		32.464 -16		4.28 -		4.51	17.14			96.1 97.2	12.6	79
	12 31	-0		11 30.028 -16		31.892 -16		4.27 -		4.52	17.12			98.3	12.4	94
1987		•0		11 29.439 -16		31.303 -16		4.26 -		4.53	17.10			99.3	12.4	
1987	1 2	•0		11 28.632 -16		30.696 -16	-	4.26 -		4.54	17.08				12.3	
1987	1 3	-0	2446798.5	11 28.208 -16		30.073 -16		4.25 -		4.55	17.06				12.2	
1987		.0		11 27.568 -16		29.432 -16	34.43	4.24 -	12.78	4.56	17.05				12.2	
1987		•0		11 26.910 -16				4.23 -		4.57	17.03				12.1	157
1987		•0		11 26.236 -16				4.23 -		4.58	17.01				12.0	
1987		•0		11 25.544 -16				4.22 -		4.59	16.99				11-9	
1987 1987		-0		11 24.836 -16		26.695 -16		4.21 -		4.60	16.97				11.8	
1987		•0		11 24.112 -10 11 23.371 -16				4.21 -		4.61	16.96				11.7	
1987		•0		11 22.614 -16				4.20 - 4.19 -		4-62				109.2	11.6	
1987		.0		11 21.840 -16				4.19 -		4-63 4-64	16.92				11.5	
1987		-0		11 21-051 -16		22.913 -16		4.18 -		4.65	16.88				11.3	91
1987		.0		11 20.246 -16				4.17 -		4.66	16.37				11.2	79
1987	1 15	-0		11 19.425 -16		21.287 -16		4.17 -		4.67	14.85				11.0	68
1987	1 16	-0	2446811.5	11 18.589 -16		20.451 -16				4.68	16.83	_			10.9	57
1987		• 0	2446812.5	11 17.738 -16	23.71 11	19.595 -16	35.82	4.16	-9.79	4.69	16.81	14.2	17.3	117,1	10.8	46
1987	-	•0		11 16.872 -16		18.733 -16				4.70	16.80	14.2	17.3	118.2	10.6	36
1987		•0		11 15.991 -16		17.851 -16				4.70	16.78				10.5	27
1987		•0		11 15.096 -16	-	13.956 -16				Z.71				120.4	10.4	21
1987 1987		•0		11 14.186 -16		16-046 -16				4.72	16.74				10.2	22
1987		•0		11 13.263 -16 11 12.326 -16		15.122 -16				4.73	16.73				10.1	29
1987		.0		11 11.376 -16		14.185 -16 13.234 -16				4.74	16.71				9.9	39
1987		.0	2446820.5			12.271 -16				4.75 4.76	16.67				9.8 9.6	51 64
1987		•0	2446821.5			11-295 -16				4.77	16.66				9.5	78
1987	1 27	•0	2446822.5			10.306 -16				4.78	16.64				9.3	
1987		•0	2446823.5							4.79				129.4	9.1	
1987		•0	2446824.5		3.96 11					4.80	16.61					120
1987		•0	2446825.5			7.272 -16	13.36	4-10		4.81				131.7	8.8	
1987		•0	2446826.5							4.82				132.8	8.6	
1987		-0	2446827.5				7.63			4.83	16.56	14.4	17.4	133.9	8.5	
1987		•0	2446828.5							4.84				135-0	8.3	158
1987	2 3	•0	2446829.5	11 1.227 -15	49.32 11	3-081 -16	1.30	4.09	-2.78	4.85	16.52	14.5	17.4	136-1	5.1	152

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